# CoolSET™-F1

TDA 16831-4

Off-Line SMPS Controller with 600V CoolMOS™ on Board

Power Management & Supply



#### TDA 16831-4

Revision History:		2002-08-08	Datasheet			
Previous Ve	ersion:	1999-12-10				
Page Subjects (major changes since last revision)						
4 Update of available types.						

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## TDA 16831-4



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# Off-Line SMPS Controller with 600 V Sense CoolMOS™ on Board

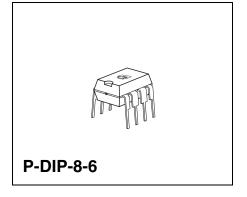
#### TDA 16831-4

#### **CoolSET**

## 1 Overview

#### 1.1 Features

- PWM controller + sense CoolMOS attached in one compact package
- 600 V avalanche rugged CoolMOS
- Typical  $R_{\rm DSon}$  = 0.5 ... 3.5  $\Omega$  at  $T_{\rm i}$  = 25°C
- Only 4 active Pins
- Standard DIP-8 Package for Output Power ≤40 W
- · Only few external components required
- Low start up current
- · Current mode control
- Input Undervoltage Lockout
- Max. Duty Cycle limitation
- Thermal Shutdown
- Modulated Gate Drive for low EMI





P-DSO-14-11

Туре	Ordering Code	Package
TDA 16831	Q67000-A9420	P-DIP-8-6
TDA 16832	Discontiued <sup>1)</sup>	P-DIP-8-6
TDA 16833	Q67000-A9389	P-DIP-8-6
TDA 16834	Discontiued <sup>1)</sup>	P-DIP-8-6
TDA 16831G	Q67000-A9421	P-DSO-14-11
TDA 16832G	Discontiued <sup>1)</sup>	P-DSO-14-11
TDA 16833G	Q67000-A9419	P-DSO-14-11

Last ordering:28.02.2003
 Last delivery:31.08.2003



Device	Output Power Range/Required Heatsink <sup>1)</sup>					
	$V_{in}$ = 85-270 VAC	$V_{in}$ = 190-265 VAC				
TDA 16831	10 W / no heatsink	10 W / no heatsink				
TDA 16832	20 W / 6 cm <sup>2</sup>	20 W / no heatsink				
TDA 16833	30 W / 3 cm <sup>2</sup>	40 W / no heatsink				
TDA 16834	40 W / 3 cm <sup>2</sup>	40 W / no heatsink				
TDA 16831G	10 W / no heatsink	10 W / no heatsink				
TDA 16832G	20 W / 8 cm <sup>2</sup>	20 W / no heatsink				
TDA 16833G	20 W / no heatsink	40 W / 3 cm <sup>2</sup>				

 $T_{A} = 70^{\circ}$ C

## 1.2 Pin Configurations

## 1.2.1 P-DIP-8-6 for Applications with $P_{\text{OUT}} \le 40 \text{ W}$ : TDA 16831/2/3/4

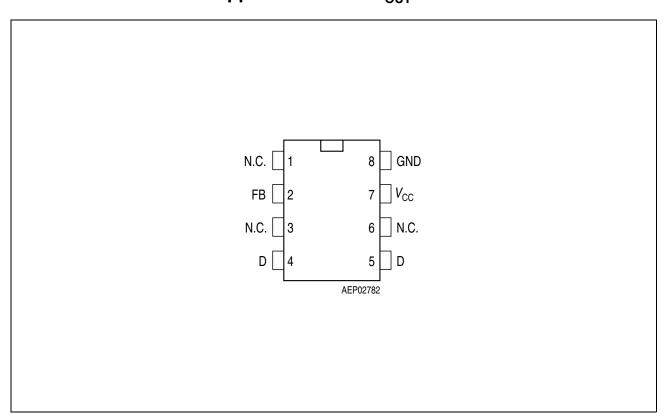


Figure 1 TDA 16831/2/3/4

### **Pin Definitions and Functions**

Pin	Symbol	Function
1	N.C.	Not Connected
2	FB	PWM Feedback Input
3	N.C.	Not Connected
4	D	600 V Drain CoolMOS
5	D	600 V Drain CoolMOS
6	N.C.	Not Connected
7	$V_{CC}$	PWM Supply Voltage
8	GND	PWM GND and Source of CoolMOS



## 1.2.2 P-DSO-14-11 for Applications with $P_{\text{OUT}} \le 20 \text{ W}$ : TDA 16831G/2G/3G

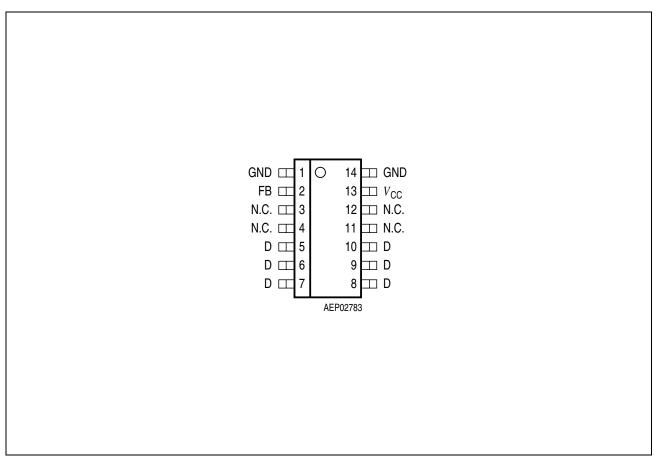


Figure 2 TDA 16831G/2G/3G

### **Pin Definitions and Functions**

Pin	Symbol	Function
1	GND	PWM GND and CoolMOS Source
2	FB	PWM Feedback Input
3	N.C.	Not Connected
4	N.C.	Not Connected
5, 6, 7	D	600 V Drain CoolMOS
8, 9, 10	D	600 V Drain CoolMOS
11	N.C.	Not Connected
12	N.C.	Not Connected
13	$V_{\sf CC}$	PWM Supply Voltage
14	GND	PWM GND and Source of CoolMOS



## 1.3 Block Diagram

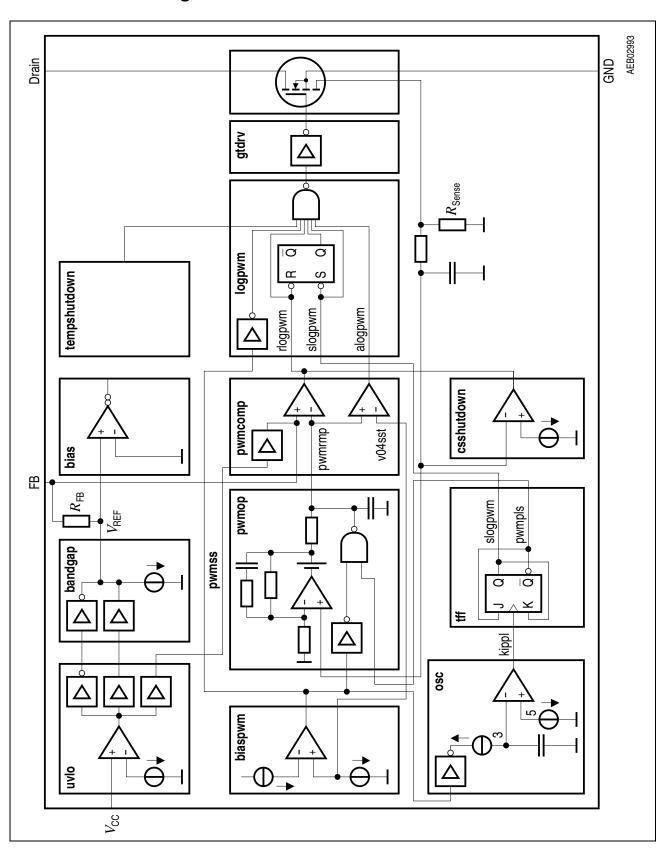


Figure 3 Block Diagram



## 2 Circuit Description

The TDA 16831-4 is a current mode pulse width modulator with integrated sense CoolMOS transistor. It fulfills the requirements of minimum external control circuitry for a flyback application.

Current mode control means that the current through the MOS transistor is compared with a reference signal derived from the output voltage of the flyback application. The result of that comparison determines the on time of the MOS transistor.

To minimize external circuitry the sense resistor which gives information about MOS current is integrated. The oscillator resistor and capacitor which determine the switching frequency are integrated, too. Special efforts have been made to compensate temperature dependency and to minimize tolerances of this resistor.

The circuit in detail: (see Figure 3)

#### **Start Up Circuit (uvlo)**

Uvlo is monitoring the external supply voltage  $V_{\rm CC}$ . When  $V_{\rm CC}$  is exceeding the on threshold  $V_{\rm CCH}$  = 12 V, the bandgap, the bias circuit and the soft start circuit are switched on. When  $V_{\rm CC}$  is falling below the off-threshold  $V_{\rm CCL}$  = 9 V the circuit is switched off. During start up the current consumption is about 30  $\mu$ A.

### Bandgap (bg)

The bandgap generates an internal very accurate reference voltage of 5.5 V to supply the internal circuits.

#### **Current Source (bias)**

The bias circuit provides the internal circuits with constant current.

#### Oscillator (osc)

The oscillator is generating a frequency twice the switching frequency  $f_{\rm switch} = 100$  kHz. Resistor, capacitor and current source which determine the frequency are integrated. The charging and discharging current of the implemented oscillator capacitor is internally trimmed, in order to achieve a very accurate switching frequency. Temperature coefficient of switching frequency is very low (see Page 18).

#### Divider Flip Flop (tff)

Tff is a flip flop which divides the oscillator frequency by one half to create the switching frequency. The maximum duty cycle is set to Dmax = 0.5.



### **Current Sense Amplifier (pwmop)**

The positive input of the pwmop is applied to the internal sense resistor. With the internal sense resistor ( $R_{\text{sense}}$ ) the sensed current coming from the CoolMOS is converted into a sense voltage. The sense voltage is amplified with a gain of 32 dB. The amplified sense voltage is connected to the negative input of the pwm comparator. Each time when the CoolMOS transistor is switched on, a current spike is superposed to the true current information. To eliminate this current spike the sense voltage is smoothed via an internal resistor capacitor network with a time constant of  $T_{d1} = 100$  ns. This is the first leading edge blanking and only a small spike is left. To reduce this small spike the current sense amplifier is creating a virtual ramp at the output. This is done by a second resistor capacitor network with  $T_{d2}$  = 100 ns and an op-offset of 0.8 V which is seen at the output of the amplifier. When gate drive is switched off the output capacitor is discharged via pulse signal pwmpls. The oscillator signal slogpwm sets the RS-flip-flop. The gate drive circuit is switched on, when capacitor voltage exceeds the internal threshold of 0.4 V. This leads to a linear ramp, which is created by the output of the amplifier. Therefore duty cycle of 0% is possible. The amplifier is compensated through an internal compensation network.

The transfer function of the amplifier can be described as

$$\frac{V_o}{V_i} = \frac{K_i}{p \times (1 + T \times p)}; p = j\omega$$

the step response is described with

$$V_{o} = V_{i} \times K_{i} \times \left(t_{on} - T + T \times e^{\frac{-t_{on}}{T}}\right)$$

$$K_{i} = \frac{40}{t_{on}}$$

### **Comparator (pwmcomp)**

T = 850 ns

The comparator pwmcomp compares the amplified current signal pwmrmp of the CoolMOS with the reference signal pwmin. Pwmin is created by an external optocoupler or external transistor and gives the information of the feedback circuitry. When the pwmrmp exceeds the reference signal pwmin the comparator switches the CoolMOS off.



### Logic (logpwm)

The logic logpwm comprises a RS-flip-flop and a NAND-gate. The NAND-gate insures that CoolMOS transistor is only switched on when sosta is on <u>and</u> pwmin has exceeded minimum threshold <u>and</u> pwmin is below pwmrmp <u>and</u> currentshutdown is off <u>and</u> tempshutdown is off <u>and</u> tff sets the starting impulse. CoolMOS transistor is switched off when pwmrmp exceeds pwmin <u>or</u> duty cycle exceeds 0.5 <u>or</u> pwmcs exceeds  $I_{\text{max}}$  <u>or</u> silicon temperature exceeds  $T_{\text{max}}$  <u>or</u> uvlo is going below threshold. The RS-flip-flop ensures that with every frequency period only one switch on can occur (double pulse suppression).

#### **Gate Drive (gtdrv)**

Gtdrv is the driver circuit for the CoolMOS and is optimized to minimize EMI influences and to provide high circuit efficiency. This is done by smoothing the switch on slope when reaching the CoolMOS threshold. Leading switch on spike is minimized then. When CoolMOS is witched off, the falling slope of the gate driver is slowed down when reaching 2 V. So an overshoot below ground can't occur. Also gate drive circuit is designed to eliminate cross conduction of the output stage.

#### **Current Shut Down (cssd)**

Current shut down circuit switches the CoolMOS immediately off when the sense current is exceeding an internal threshold of 100 mV at  $R_{\rm sense}$ .

### Tempshutdown (tsd)

Tempshutdown switches the CoolMOS off when junction temperature of the PWM controller is exceeding an internal threshold.



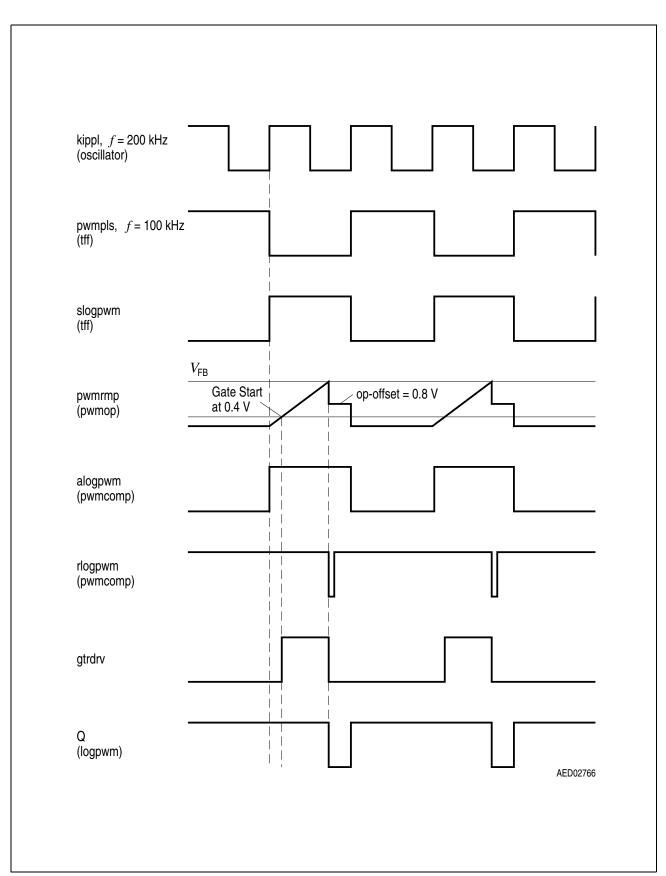


Figure 4 Signal Diagram



## 3 Electrical Characteristics

## 3.1 Absolute Maximum Ratings

Parameter	Symbol	Limit Values		Unit	Remarks	
		min.	max.			
Supply Voltage	$V_{\sf CC}$	-0.3	$V_{Z}$	V	Zener Voltage <sup>1)</sup>	
Supply + Zener Current	$I_{CCZ}$	0	20	mA	Page 14 Beware of $P_{\text{max}}^{2}$	
Drain Source Voltage	$V_{DS}$		600	V		
Avalanche Current	$I_{AC}$		I <sub>csthmax</sub>	Α	<i>t</i> = 100 ns	
Voltage at FB	$V_{FB}$	-0.3	5.5	V		
Junction Temperature	$T_{\rm j}$	-40	150	°C		
Storage Temperature	$T_{stg}$	-50	150			
Thermal Resistance	$R_{thSA}$		90	K/W	P-DIP-8-6	
System-Air			125		P-DSO-14-11	

 $<sup>^{\</sup>scriptscriptstyle 1)}$  Be aware that  $V_{\rm CC}$  capacitor is discharged before IC is plugged into the application board.

## 3.2 Operating Range

Parameter	Symbol	Limit Values		Unit	Remarks
		min.	max.		
Supply Voltage	$V_{\sf CC}$	$V_{CCH}$	$V_{Z}$	V	
Junction Temperature	$T_{j}$	-25	120	°C	

<sup>&</sup>lt;sup>2)</sup> Power dissipation should be observed.



## 3.3 Supply Section

-25°C <  $T_{\rm j}$  < 120°C,  $V_{\rm CC}$  = 15 V

Parameter	Symbol	Limit Values			Unit	<b>Test Conditions</b>
		min.	typ.	max.		
Quiescent Current	$I_{CCL}$		25	80	μΑ	
Supply Current Active	$I_{CCHA}$		4.5	6	mA	TDA 16831/2/G
			6	7.5		TDA 16833/G
			7	8.5		TDA 16834
$\overline{V_{ m CC}}$ Turn-On Threshold	$V_{CCH}$		12	12.5	V	
$\overline{V_{\rm CC}}$ Turn-Off Threshold	$V_{CCL}$	8.5	9			
$\overline{V_{\rm CC}}$ Turn-On/Off Hysteresis	$V_{CCHY}$		3			
$\overline{V_{\rm CC}}$ Zener Clamp	$V_{Z}$	16	17.5	19		
Controller Thermal Shutdown	$T_{jSD}$	120	135	150	°C	TDA 16831/2/3/G/4
Thermal Hysteresis	$T_{jHy}$		2			

## 3.4 Oscillator Section

-25°C <  $T_{\rm j}$  < 120°C,  $V_{\rm CC}$  = 15 V

Parameter	Symbol	I Limit Values		Unit	<b>Test Conditions</b>	
		min.	typ.	max.		
Accuracy	f	90	100	110	kHz	
Temperature Coefficient	TK f		1000		ppm/°C	



### 3.5 PWM Section

Parameter	Symbol	Limit Values			Unit	<b>Test Conditions</b>
		min.	typ.	max.		
Duty Cycle	D	0		0.5		
Transimpedance	$Z_{PWM}$		4		V/A	TDA 16831/G
$\Delta V_{FB}$ / $\Delta I_{Drain}^{1}$			2			TDA 16832/G
			1.3			TDA 16833/G/4
OP Gain Bandwidth <sup>2)</sup>	Bw		2		MHz	
OP Phase Margin <sup>2)</sup>	Phi <sub>m</sub>		70		Degree	
$\overline{V_{\mathrm{FB}}}$ Operating Range min. Level	$V_{FBmin}$	0.45		0.85	V	for D = 0
$\overline{V_{\mathrm{FB}}}$ Operating Range max. Level	$V_{FBmax}$	3.5		4.8		$I_{\rm cs} = 0.95 I_{\rm csth}$
Feedback Resistance	$R_{FB}$	3.0	3.7	4.9	ΚΩ	
Temperature Coefficient $R_{FB}$	$R_{FBTK}$		600		ppm/°C	
Internal Reference Voltage	$V_{refint}$	5.3	5.5	5.7	V	
Temperature Coefficient $V_{\rm refint}$	$V_{reftk}$		0.2		mV/°C	

 $<sup>^{\</sup>scriptscriptstyle 1)}$   $\,$  For discontinuous mode the  $V_{\rm FB}$  is described by:

$$V_{\text{FB}} = Z_{\text{PWM}} \times \frac{I_{\text{PK}}}{t_{\text{on}}} \times \left(t_{\text{on}} - T_1 + T_1 \times e^{\frac{-t_{\text{on}}}{T_1}}\right) + 0.6 \times \left(1 - e^{\frac{-t_{\text{on}}}{T_2}}\right)$$

 $T_1 = 850 \text{ ns}; T_2 = 200 \text{ ns}$ 

<sup>&</sup>lt;sup>2)</sup> Guaranteed by design

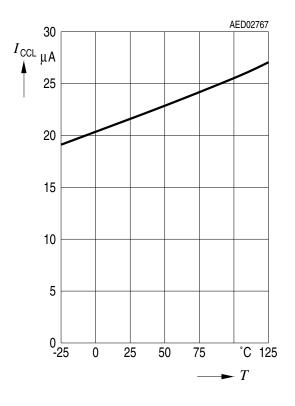


## 3.6 Output Section

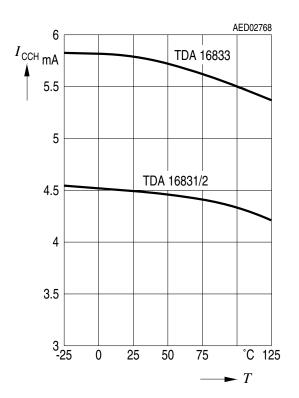
Parameter	Symbol	Liı	Limit Values		Unit	<b>Test Conditions</b>	
		min.	typ.	max.			
Drain Source Breakdown Voltage $T_A = 25^{\circ}\text{C}$	$V_{(\mathrm{BR})\mathrm{DSS}}$	600			V		
Drain Source On-Resistance	$R_{DSon}$		3.5		Ω	TDA 16831/2/G	
$T_{A} = 25^{\circ}C$			1			TDA 16833/G	
			0.5			TDA 16834	
Drain Source On-Resistance	$R_{DSon}$			9	Ω	TDA 16831/2/G	
$-25 < T_A < 120^{\circ}C$				2.7		TDA 16833/G	
				1.6		TDA 16834	
Zero Gate Voltage Drain Current	$I_{DSS}$		0.5	50	μΑ	$V_{\rm GS} = 0$	
Output Capacitance	$C_{OSS}$		25		pF	TDA16833	
Avalanche Current	$I_{AR}$		I <sub>csthma</sub>		А	$t_{\rm DR} = 100 \; {\rm ns}$	
$I_{\text{source}}$ Current Limit Threshold	$I_{\mathrm{csth}}$	0.6	0.9	1.4	Α	TDA 16831/G	
		1.2	1.8	2.7		TDA 16832/G	
		2.2	2.9	4.8		TDA 16833/G	
		2.2	2.9	4.8		TDA 16834	
Time Constant $I_{csth}$	$t_{\rm csth}$		300		ns		
Rise Time	$t_{rise}$		70				
Fall Time	$t_{fall}$		50				



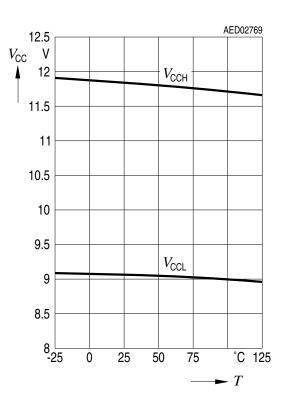
# **Quiescent Current versus Temperature**



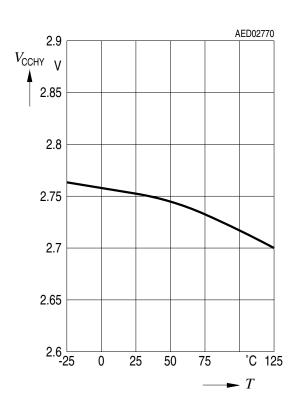
# **Supply Current Active versus Temperature**



# **Turn On/Off Supply Voltage versus Temperature**

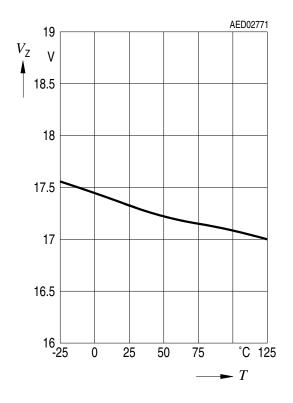


## **Turn On/Off Hysteresis**

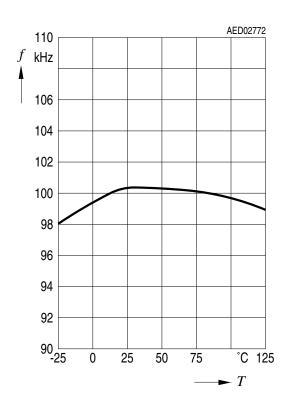




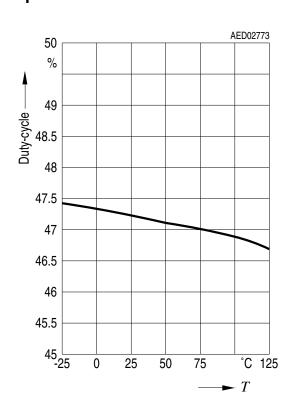
### $V_{ m CC}$ Zener Clamp



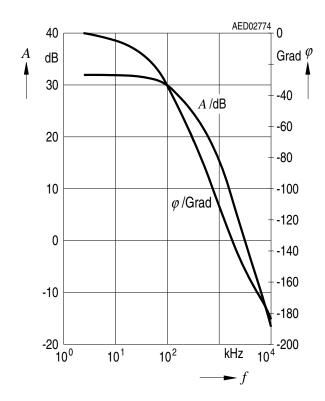
## Switching Frequency versus Temperature



## Maximum Duty Cycle versus Temperature TDA 16831/2/3/G/4

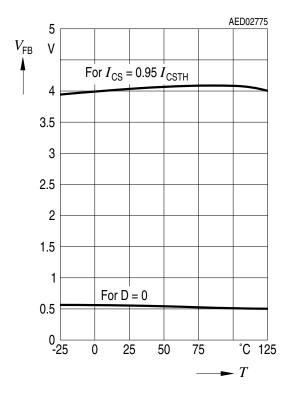


# Operational Amplifier Phase and Amplitude versus Frequency

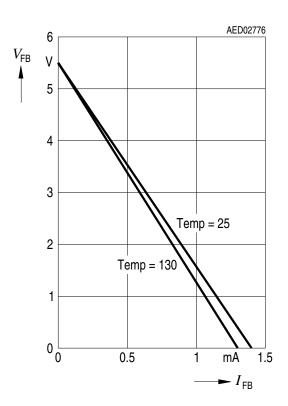




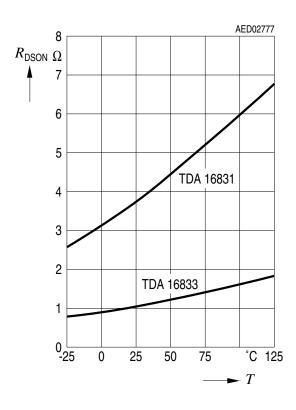
# Feedback Voltage Operating Range versus Temperature



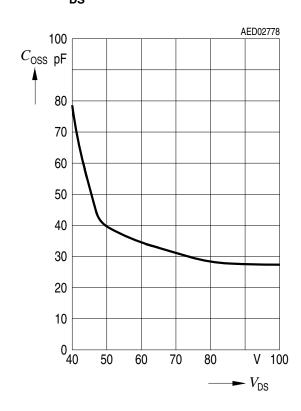
## Feedback Voltage versus Feedback Current



## $R_{\mathrm{DSon}}$ versus Temperature

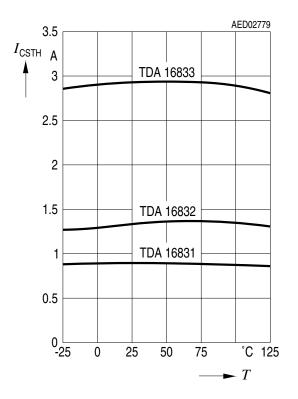


# TDA 16833 Output Capacitance $C_{\mathrm{OSS}}$ versus $V_{\mathrm{DS}}$

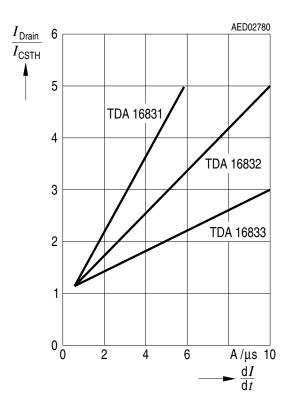




# $I_{ m source}$ Current Limit Threshold $I_{ m csth}$ versus Temperature



# Normalized Overcurrent Shutdown versus Drain Current Slope



## **Application Circuit**

## 4 Application Circuit

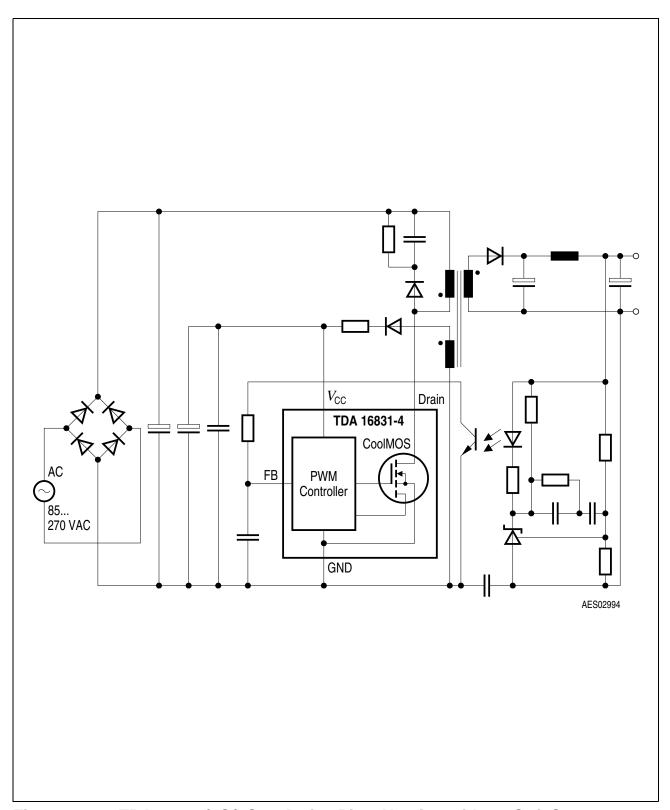
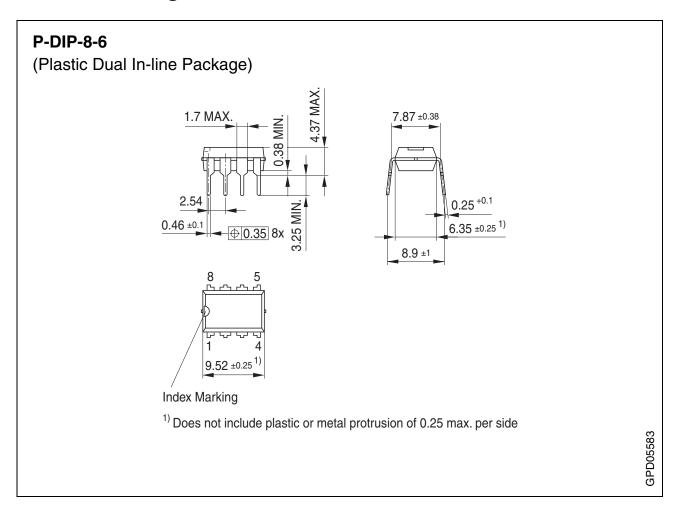


Figure 5 TDA 16832/2G/3G: 4 Active Pins, Version without Soft Start



## **Package Outlines**

## 5 Package Outlines

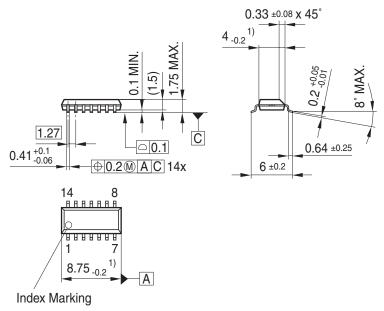




### **Package Outlines**

#### P-DSO-14-11

(Plastic Dual Small Outline)



 $<sup>^{\</sup>rm 1)}\,{\rm Does}$  not include plastic or metal protrusion of 0.15 max. per side

GPS09033

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Dimensions in mm

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