

# ZXLD1362

## 1A LED driver with internal switch

### Description

The ZXLD1362 is a continuous mode inductive step-down converter, designed for driving single or multiple series connected LEDs efficiently from a voltage source higher than the LED voltage. The device operates from an input supply between 6V and 60V and provides an externally adjustable output current of up to 1A. Depending upon supply voltage and external components, this can provide up to 48 watts of output power.

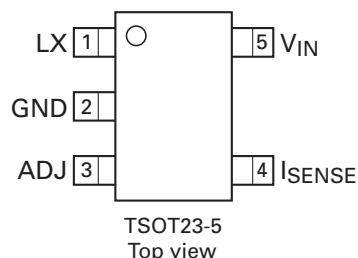
The ZXLD1362 includes the output switch and a high-side output current sensing circuit, which uses an external resistor to set the nominal average output current.

Output current can be adjusted above, or below the set value, by applying an external control signal to the 'ADJ' pin.

### Features

- Simple low parts count
- Internal 60V NDMOS switch
- Up to 1A output current
- Single pin on/off and brightness control using DC voltage or PWM
- PWM resolution up to 3000:1
- Soft start capability
- High efficiency (up to 95%)
- Wide input voltage range: 6V to 60V
- 65V transient capability
- Low power shutdown
- Up to 1MHz switching frequency
- Inherent open-circuit LED protection
- Typical 4% output current accuracy

### Pin connections



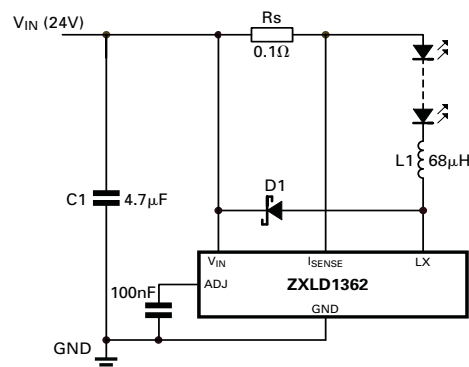
The ADJ pin will accept either a DC voltage or a PWM waveform. Depending upon the control frequency, this will provide either a continuous (dimmed) or a gated output current. Soft-start can be forced using an external capacitor from the ADJ pin to ground.

Applying a voltage of 0.2V or lower to the ADJ pin turns the output off and switches the device into a low current standby state.

### Applications

- Low voltage halogen replacement LEDs
- Automotive lighting
- Low voltage industrial lighting
- LED back-up lighting
- Illuminated signs
- Emergency lighting
- SELV lighting
- LCD TV backlighting

### Typical application circuit



## Absolute maximum ratings (voltages to GND unless otherwise stated)

Input voltage ( $V_{IN}$ )	-0.3V to +60V (65V for 0.5 sec)
$I_{SENSE}$ voltage ( $V_{SENSE}$ )	+0.3V to -5V (measured with respect to $V_{IN}$ )
LX output voltage ( $V_{LX}$ )	-0.3V to +60V (65V for 0.5 sec)
Adjust pin input voltage ( $V_{ADJ}$ )	-0.3V to +6V
Switch output current ( $I_{LX}$ )	1.25A
Power dissipation ( $P_{tot}$ )	1W
(Refer to package thermal de-rating curve on page 16)	
Operating temperature ( $T_{OP}$ )	-40 to 125°C
Storage temperature ( $T_{ST}$ )	-55 to 150°C
Junction temperature ( $T_{j MAX}$ )	150°C

These are stress ratings only. Operation outside the absolute maximum ratings may cause device failure. Operation at the absolute maximum ratings, for extended periods, may reduce device reliability.

## Thermal resistance

Junction to ambient ( $R_{\theta JA}$ )	82°C/W
Junction to case ( $R_{\theta JC}$ )	TBD

## Electrical characteristics (test conditions: $V_{IN}=24V$ , $T_{amb}=25^{\circ}C$ unless otherwise stated)<sup>(a)</sup>

Symbol	Parameter	Conditions	Min.	Typ.	Max.	Unit
$V_{IN}$	Input voltage	See note (c)	6		60	V
$V_{SD}$	Internal regulator shutdown threshold			4.7		V
$I_{INQoff}$	Quiescent supply current with output off	ADJ pin grounded		65	TBD	$\mu A$
$I_{INQon}$	Quiescent supply current with output switching	ADJ pin floating, $L=68\mu H$ , 3 LEDs, $f=260kHz$		1.8	TBD	mA
$V_{SENSE}$	Mean current sense threshold voltage (Defines LED current setting accuracy)	Measured on $I_{SENSE}$ pin with respect to $V_{IN}$ $V_{ADJ} = 1.25V$	95	100	105	mV
$V_{SENSEHYS}$	Sense threshold hysteresis			$\pm 15$		%
$I_{SENSE}$	$I_{SENSE}$ pin input current	$V_{SENSE} = V_{IN} - 0.1$		4	TBD	$\mu A$
$V_{REF}$	Internal reference voltage	Measured on ADJ pin with pin floating		1.25		V
$\Delta V_{REF} / \Delta T$	Temperature coefficient of $V_{REF}$			50		ppm/°C
$V_{ADJ}$	External control voltage range on ADJ pin for DC brightness control <sup>(b)</sup>		0.3		2.5	V
$V_{ADJoff}$	DC voltage on ADJ pin to switch device from active (on) state to quiescent (off) state	$V_{ADJ}$ falling	0.15	0.2	0.25	V

### NOTES:

- (a) Production testing of the device is performed at 25°C. Functional operation of the device and parameters specified over a -40°C to +105°C temperature range, are guaranteed by design, characterization and process control.
- (b) 100% brightness corresponds to  $V_{ADJ} = V_{ADJ(nom)} = V_{REF}$ . Driving the ADJ pin above  $V_{REF}$  will increase the  $V_{SENSE}$  threshold and output current proportionally.
- (c)  $V_{IN} > 16V$  to fully enhance output transistor. Otherwise out current must be derated - see graphs. Operation at low supply may cause excessive heating due to increased on-resistance.

# ZXLD1362

## Electrical characteristics (test conditions: $V_{IN}=24V$ , $T_{amb}=25^{\circ}C$ unless otherwise stated) (cont.)

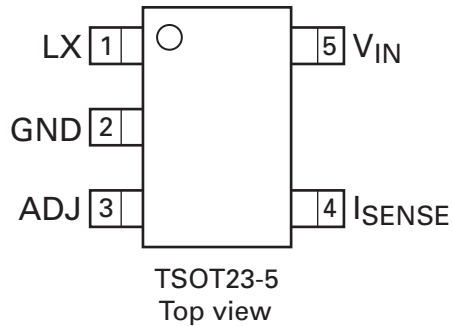
Symbol	Parameter	Conditions	Min.	Typ.	Max.	Unit
$V_{ADJ_{on}}$	DC voltage on ADJ pin to switch device from quiescent (off) state to active (on) state	$V_{ADJ}$ rising	0.2	0.25	0.3	V
$R_{ADJ}$	Resistance between ADJ pin and $V_{REF}$	$0 < V_{ADJ} < V_{REF}$ $V_{ADJ} > V_{REF} + 100mV$	30 13.5	50 20	65 25	$k\Omega$
$I_{LX_{mean}}$	Continuous LX switch current				1	A
$R_{LX}$	LX Switch 'On' resistance	@ $I_{LX} = 1 A$		0.5	1.0	$\Omega$
$I_{LX(leak)}$	LX switch leakage current				5	$\mu A$
$D_{P_{PWM(LF)}}$	Duty cycle range of PWM signal applied to ADJ pin during low frequency PWM dimming mode	PWM frequency < 300Hz PWM amplitude = $V_{REF}$	0.001		1	
	Brightness control range	Measured on ADJ pin		1000:1		
$DC_{ADJ}^{(*)}$	DC Brightness control range	See note (*)		5:1		
$T_{SS}$	Soft start time	Time taken for output current to reach 90% of final value after voltage on ADJ pin has risen above 0.3V Requires external capacitor 22nF. See graphs for more details		2		ms
$f_{LX}$	Operating frequency (See graphs for more detail)	ADJ pin floating $L = 68\mu H (0.1\Omega)$ $I_{OUT} = 1A @ V_{LED} = 3.6V$ Driving 3 LEDs		260		KHz
$T_{ONmin}$	Minimum switch 'ON' time	LX switch 'ON'		240 (†)	TBD	ns
$T_{OFFmin}$	Minimum switch 'OFF' time	LX switch 'OFF'		200 (†)	TBD	ns
$T_{ONmin\_REC}$	Recommended minimum switch 'ON' time	LX switch 'ON'		800		ns
$f_{LXmax}$	Recommended maximum operating frequency				1	MHz
$D_{LX}$	Recommended duty cycle range of output switch at $f_{LXmax}$		0.3		0.7	
$T_{PD}$	Internal comparator propagation delay			50		ns

### NOTES:

(\*) Ratio of maximum brightness to minimum brightness before shutdown  $V_{REF} = 1.25/0.3$ .  $V_{REF}$  externally driven to 2.5V, ratio 10:1.

(†) Parameters are not tested at production. Parameters are guaranteed by design, characterization and process control.

## Pin description



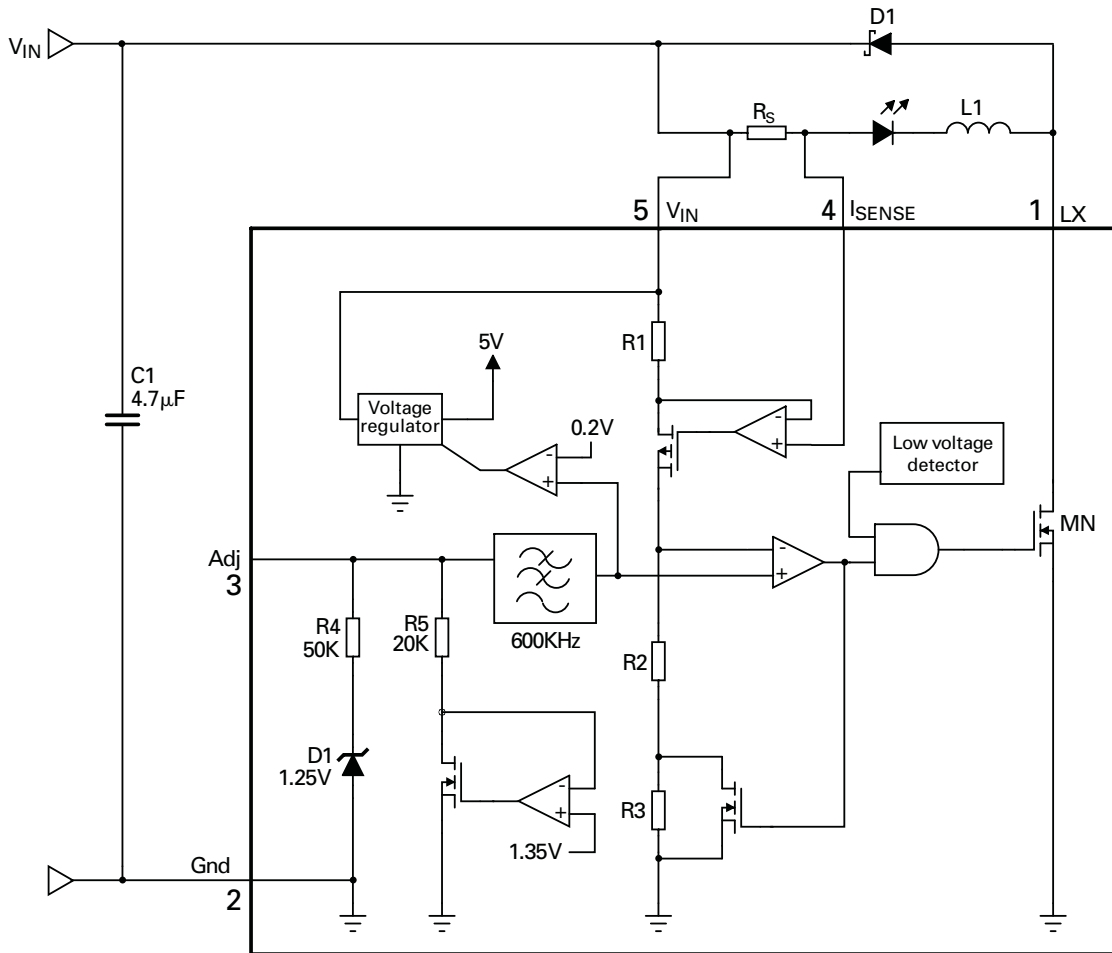
Name	Pin no.	Description
LX	1	Drain of NDMOS switch
GND	2	Ground (0V)
ADJ	3	Multi-function On/Off and brightness control pin: <ul style="list-style-type: none"> <li>• Leave floating for normal operation. (<math>V_{ADJ} = V_{REF} = 1.25V</math> giving nominal average output current <math>I_{OUTnom} = 0.1/R_S</math>)</li> <li>• Drive to voltage below 0.2V to turn off output current</li> <li>• Drive with DC voltage (<math>0.3V &lt; V_{ADJ} &lt; 2.5V</math>) to adjust output current from 25% to 200% of <math>I_{OUTnom}</math></li> <li>• Connect a capacitor from this pin to ground to set soft-start time. Soft start time increases approximately 0.2ms/nF</li> </ul>
$I_{SENSE}$	4	Connect resistor $R_S$ from this pin to $V_{IN}$ to define nominal average output current $I_{OUTnom} = 0.1/R_S$ ( <b>Note:</b> $R_{Smin} = 0.1\Omega$ with ADJ pin open-circuit)
$V_{IN}$	5	Input voltage (6V to 60V). Decouple to ground with 4.7 $\mu$ F or higher X7R ceramic capacitor close to device

## Ordering information

Device	Reel size (mm)	Reel width (inches)	Quantity per reel	Device mark
ZXLD1362ET5TA	180	8	3,000	1362

# ZXLD1362

## Block diagram



## Device description

The device, in conjunction with the coil (L1) and current sense resistor ( $R_S$ ), forms a self-oscillating continuous-mode buck converter.

### Device operation (Refer to block diagram and Figure 1 - Operating waveforms)

Operation can be best understood by assuming that the ADJ pin of the device is unconnected and the voltage on this pin ( $V_{ADJ}$ ) appears directly at the (+) input of the comparator.

When input voltage  $V_{IN}$  is first applied, the initial current in L1 and  $R_S$  is zero and there is no output from the current sense circuit. Under this condition, the (-) input to the comparator is at ground and its output is high. This turns MN on and switches the LX pin low, causing current to flow from  $V_{IN}$  to ground, via  $R_S$ , L1 and the LED(s). The current rises at a rate determined by  $V_{IN}$  and L1 to produce a voltage ramp ( $V_{SENSE}$ ) across  $R_S$ . The supply referred voltage  $V_{SENSE}$  is forced across internal resistor R1 by the current sense circuit and produces a proportional current in internal resistors R2 and R3. This produces a ground referred rising voltage at the (-) input of the comparator. When this reaches the threshold voltage ( $V_{ADJ}$ ), the comparator output switches low and MN turns off. The comparator output also drives another NMOS switch, which bypasses internal resistor R3 to provide a controlled amount of hysteresis. The hysteresis is set by R3 to be nominally 15% of  $V_{ADJ}$ .

When MN is off, the current in L1 continues to flow via D1 and the LED(s) back to  $V_{IN}$ . The current decays at a rate determined by the LED(s) and diode forward voltages to produce a falling voltage at the input of the comparator. When this voltage returns to  $V_{ADJ}$ , the comparator output switches high again. This cycle of events repeats, with the comparator input ramping between limits of  $V_{ADJ} \pm 15\%$ .

## Switching thresholds

With  $V_{ADJ} = V_{REF}$ , the ratios of R1, R2 and R3 define an average  $V_{SENSE}$  switching threshold of 100mV (measured on the  $I_{SENSE}$  pin with respect to  $V_{IN}$ ). The average output current  $I_{OUTnom}$  is then defined by this voltage and  $R_S$  according to:

$$I_{OUTnom} = 100\text{mV}/R_S$$

Nominal ripple current is  $\pm 15\text{mV}/R_S$

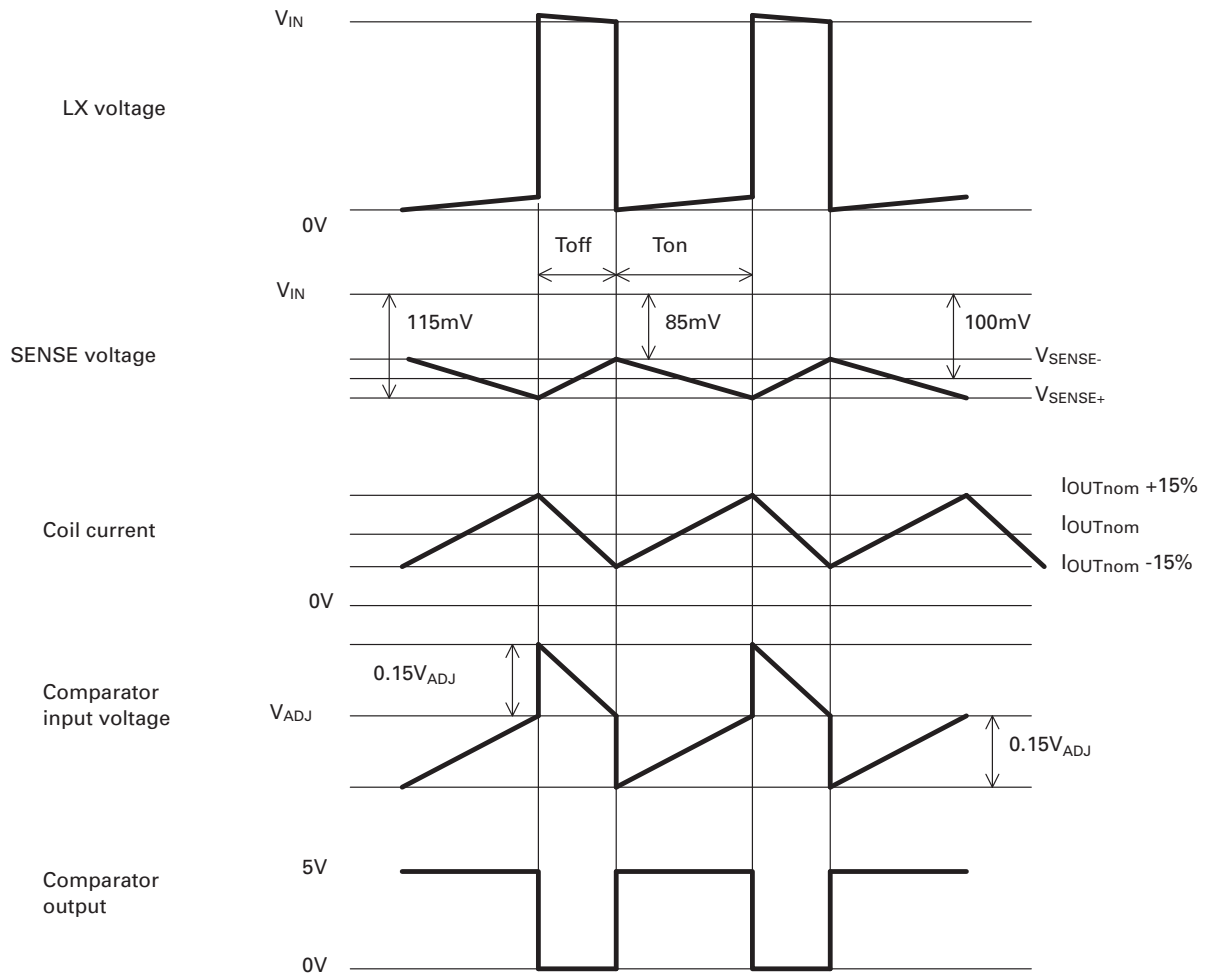
## Adjusting output current

The device contains a low pass filter between the ADJ pin and the threshold comparator and an internal current limiting resistor (50k $\Omega$  nom) between ADJ and the internal reference voltage. This allows the ADJ pin to be overdriven with either DC or pulse signals to change the  $V_{SENSE}$  switching threshold and adjust the output current.

Details of the different modes of adjusting output current are given in the applications section.

## Output shutdown

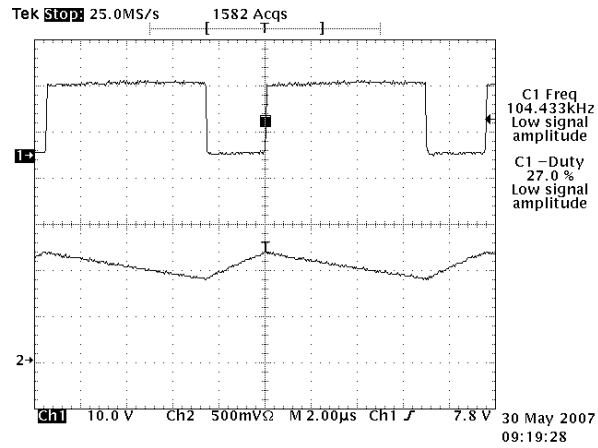
The output of the low pass filter drives the shutdown circuit. When the input voltage to this circuit falls below the threshold (0.2V nom.), the internal regulator and the output switch are turned off. The voltage reference remains powered during shutdown to provide the bias current for the shutdown circuit. Quiescent supply current during shutdown is nominally 60 $\mu\text{A}$  and switch leakage is below 5 $\mu\text{A}$ .



**Figure 1 - Operating waveforms**

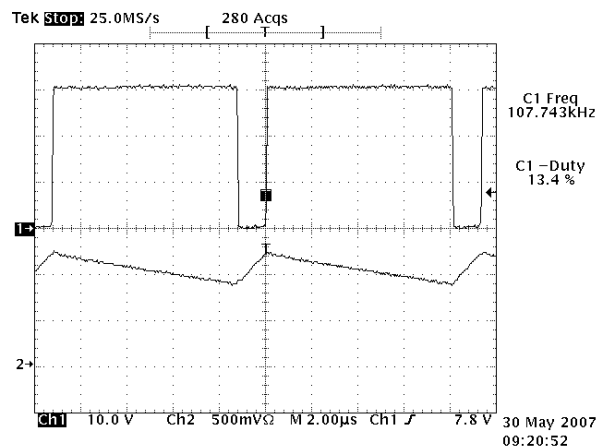
## Actual operating waveforms [ $V_{IN}=15V$ , $R_S=0.1\Omega$ , $L=100\mu H$ ]

Normal operation. Output current (Ch1) and LX voltage (Ch2)



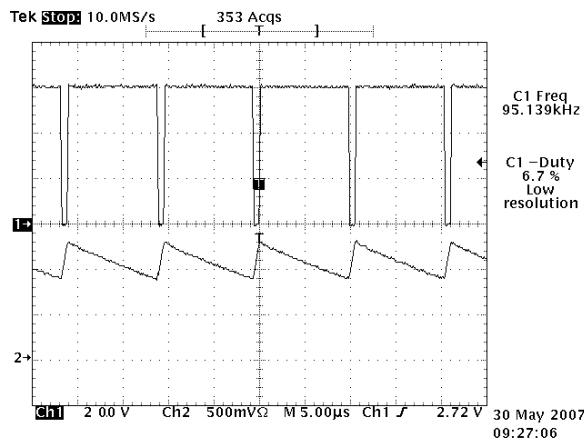
## Actual operating waveforms [ $V_{IN}=30V$ , $R_S=0.1\Omega$ , $L=100\mu H$ ]

Normal operation. Output current (Ch1) and LX voltage (Ch2)



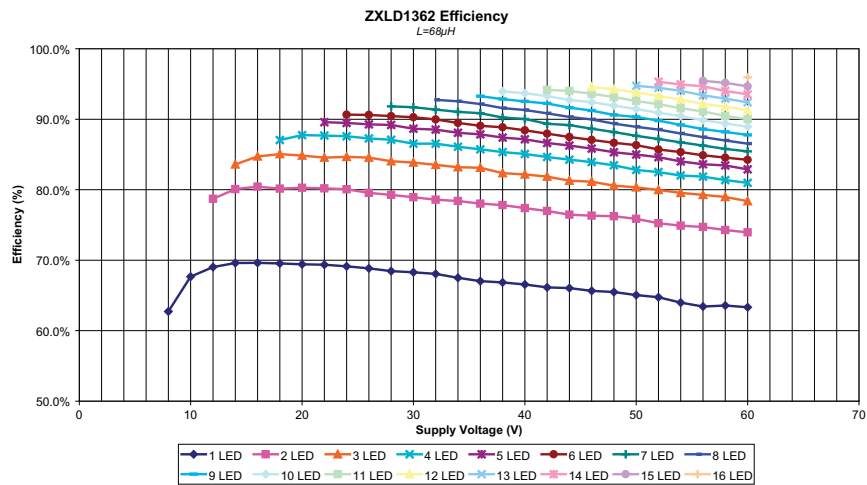
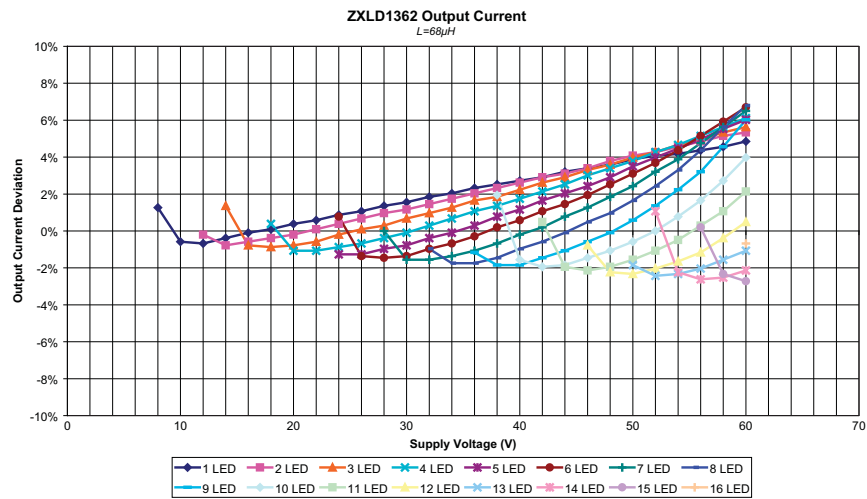
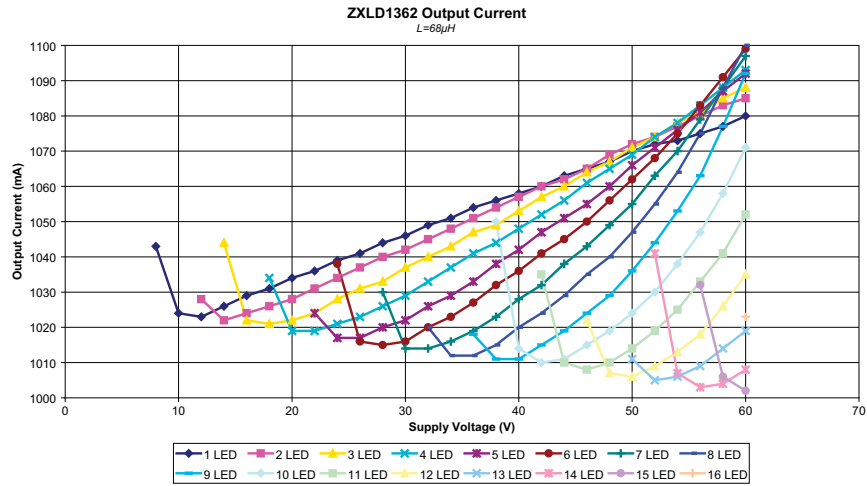
## Actual operating waveforms [ $V_{IN}=60V$ , $R_S=0.1\Omega$ , $L=100\mu H$ ]

Normal operation. Output current (Ch1) and LX voltage (Ch2)

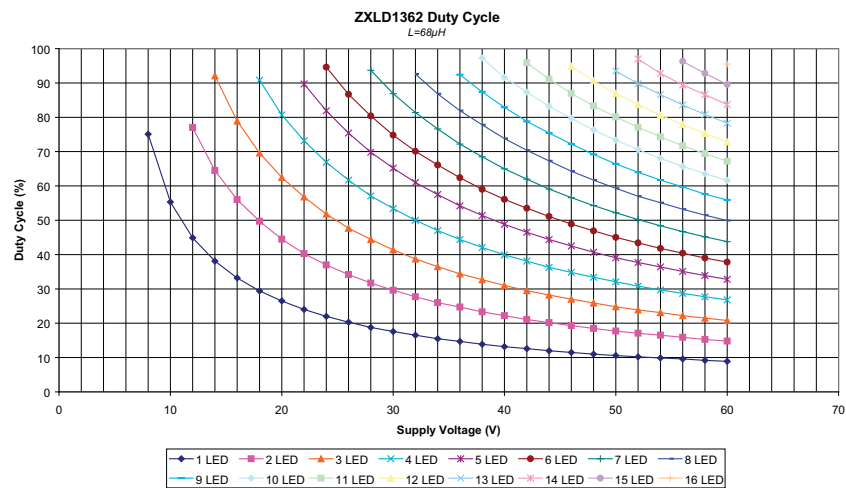
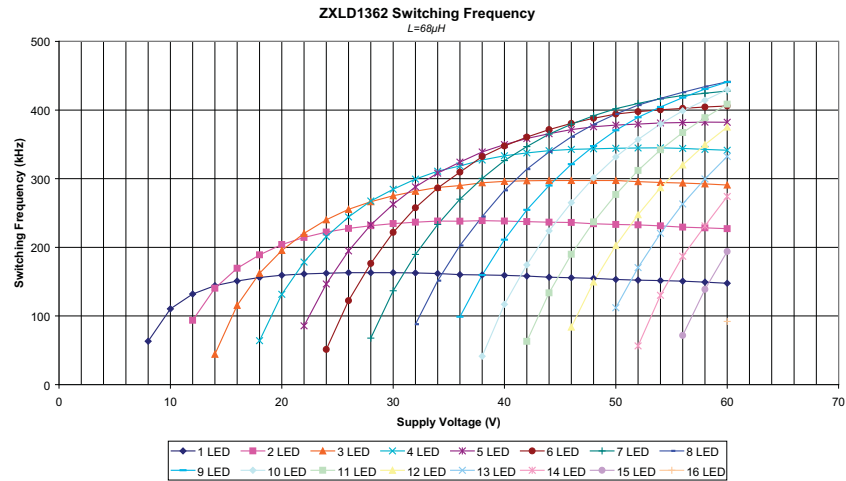




## Typical operating conditions

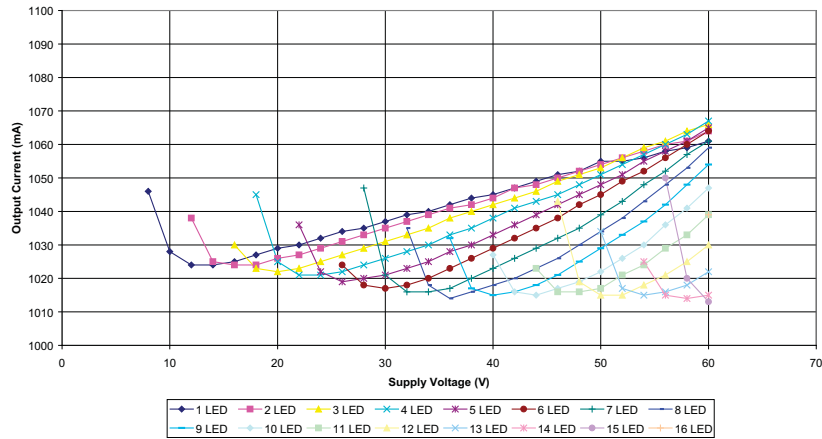


## Typical operating conditions

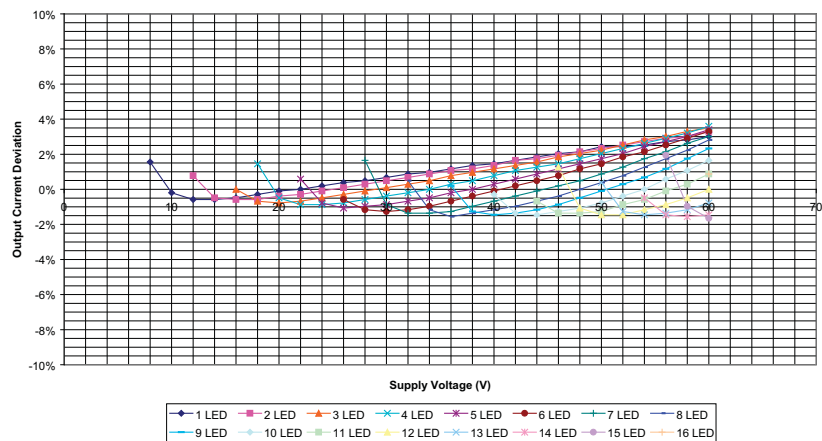


## Typical operating conditions

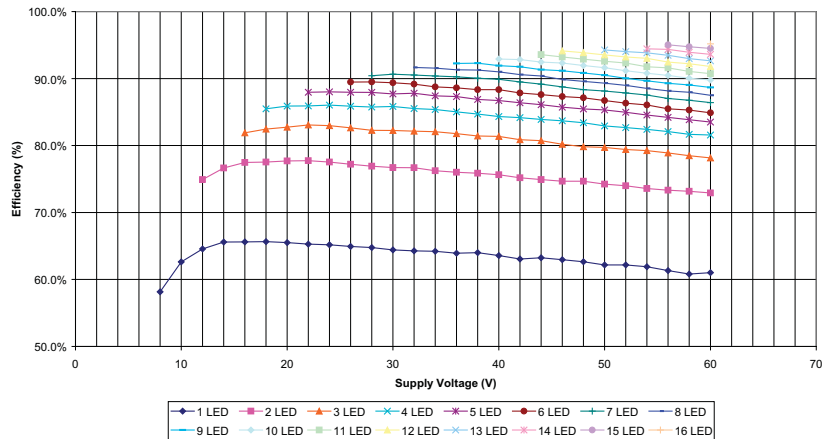
ZXLD1362 Output Current  
L=100µH



ZXLD1362 Output Current  
L=100µH

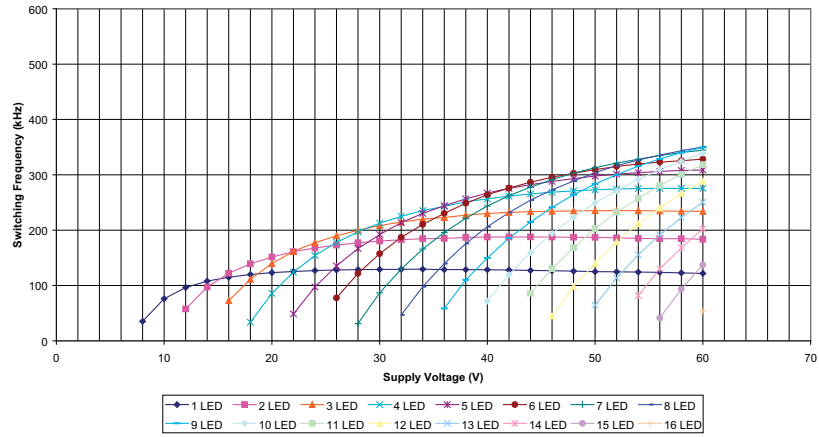


ZXLD1362 Efficiency  
L=100µH

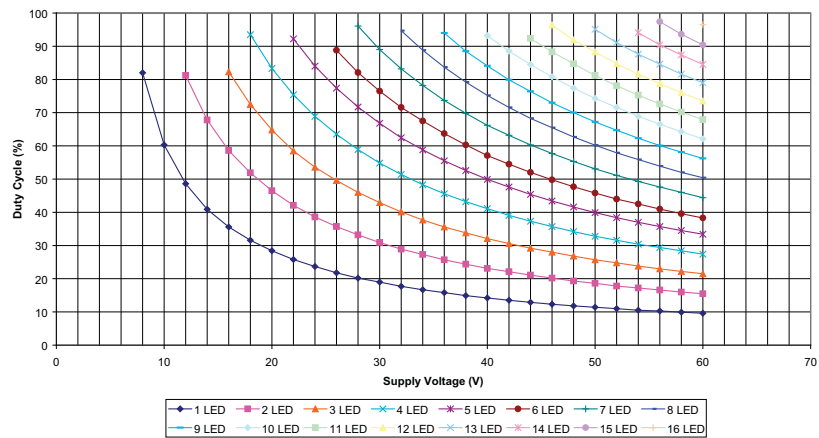


## Typical operating conditions

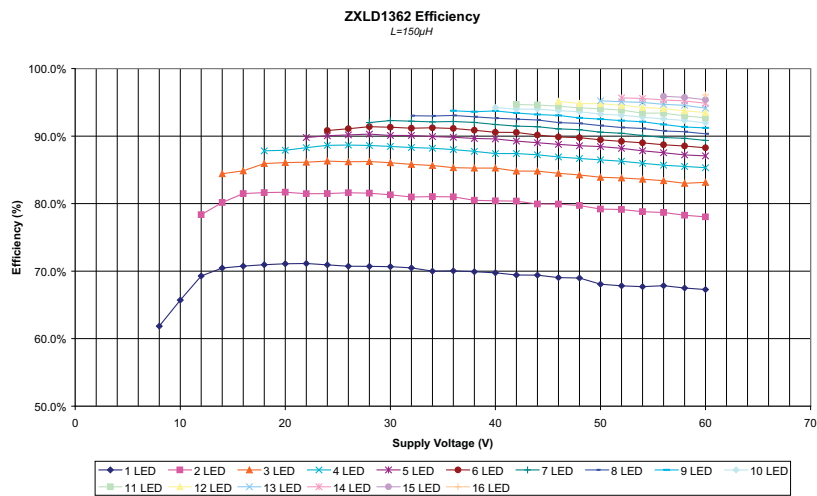
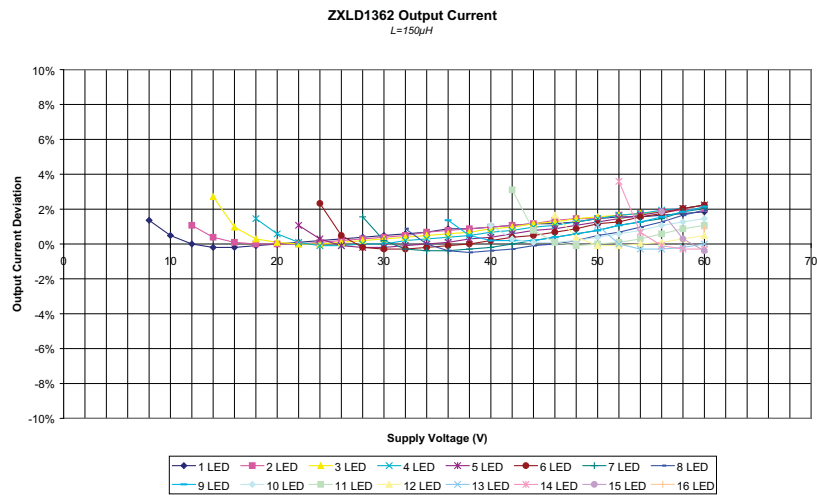
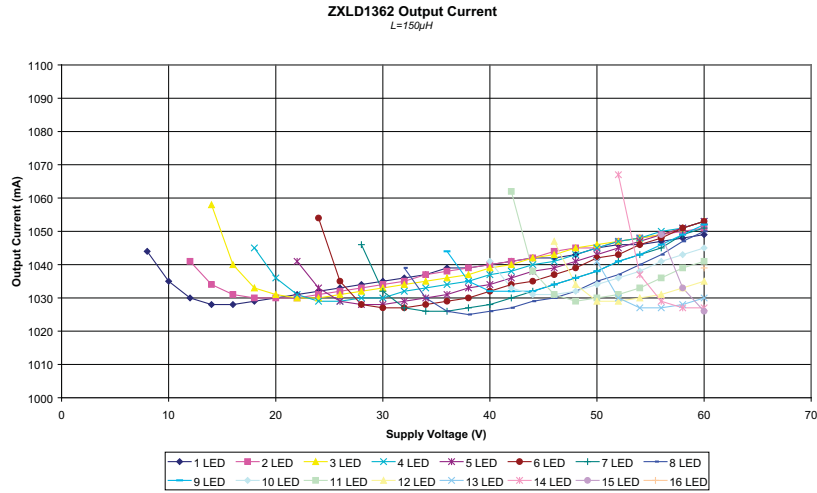
**ZXLD1362 Switching Frequency**  
L=100µH



**ZXLD1362 Duty Cycle**  
L=100µH

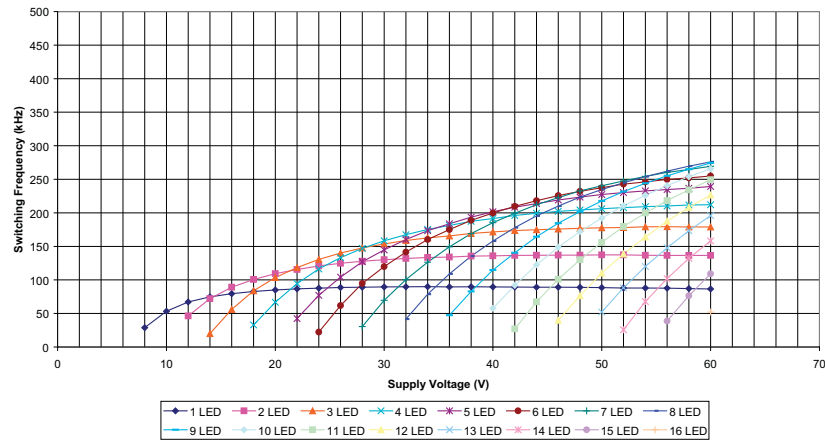


## Typical operating conditions

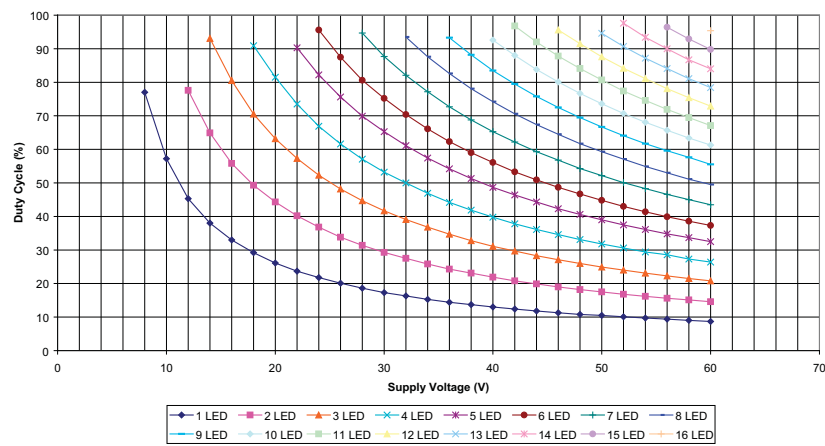


## Typical operating conditions

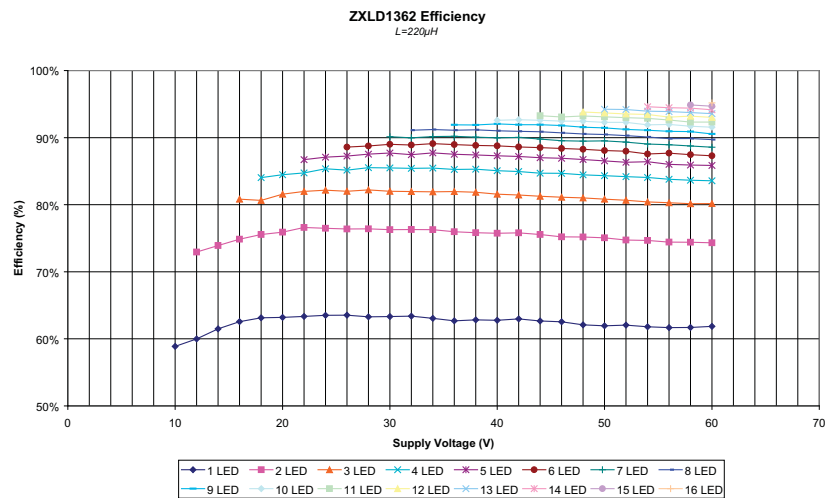
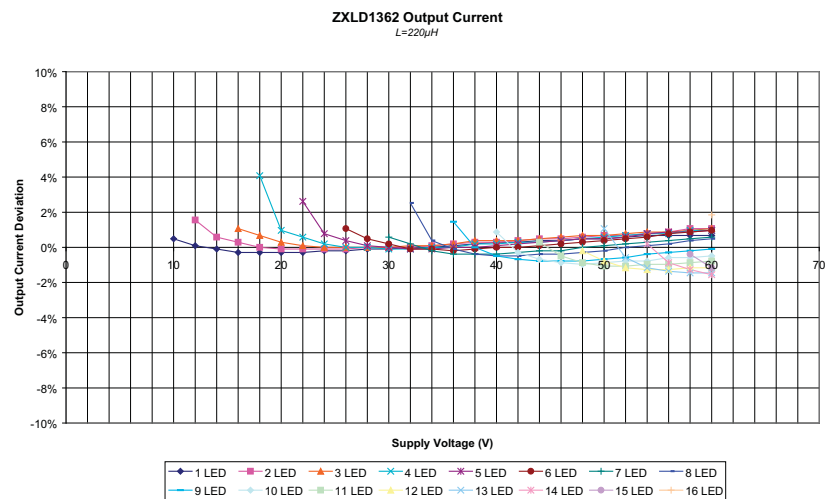
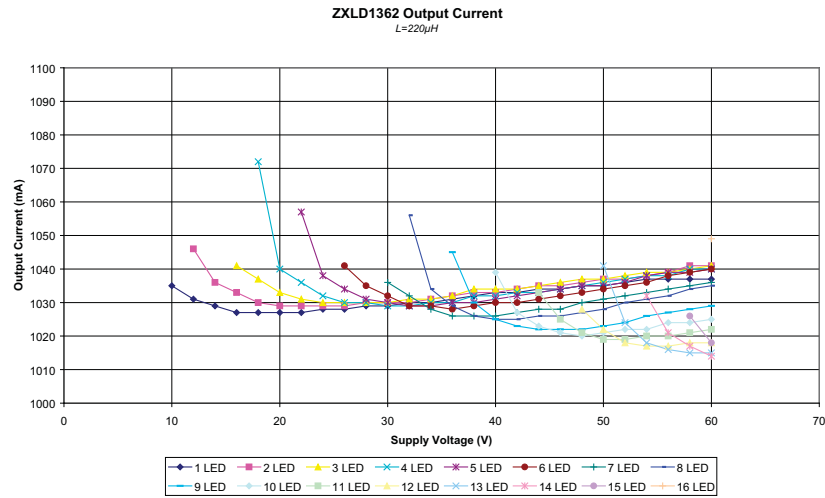
ZXLD1362 Switching Frequency  
L=150µH



ZXLD1362 Duty Cycle  
L=150µH

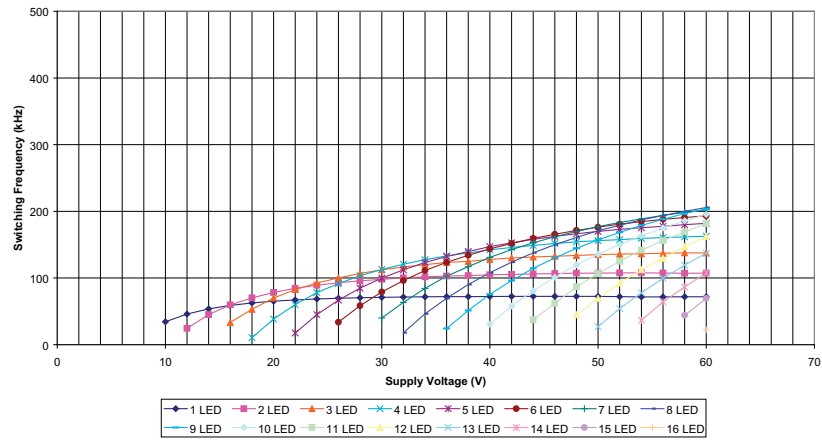


## Typical operating conditions

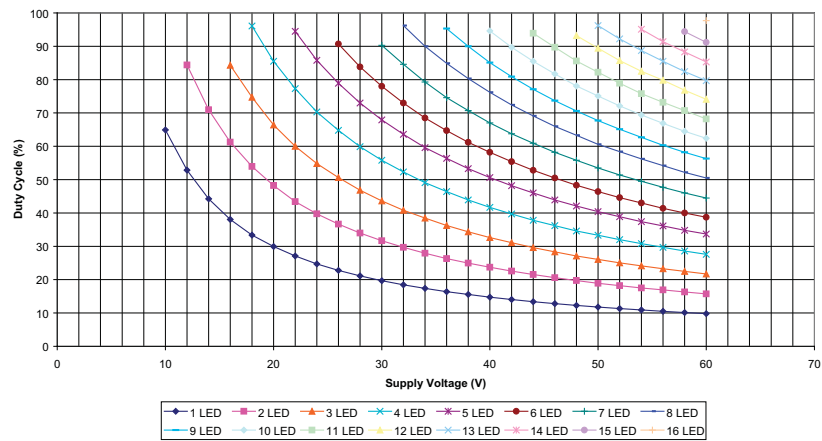


## Typical operating conditions

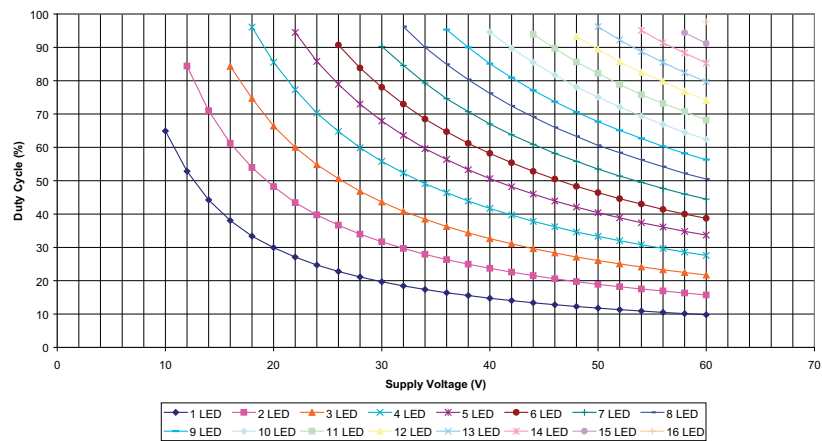
**ZXLD1362 Switching Frequency**  
*L=220µH*



**ZXLD1362 Duty Cycle**  
*L=220µH*

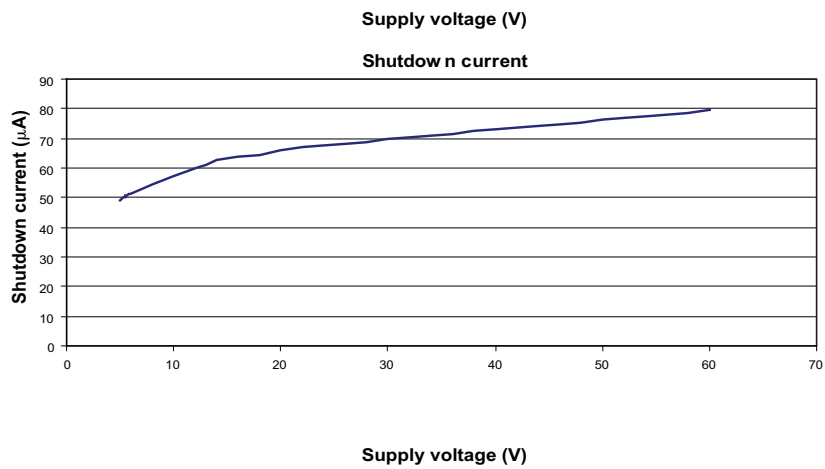
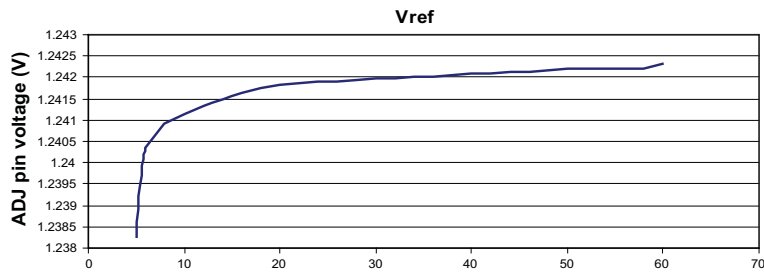
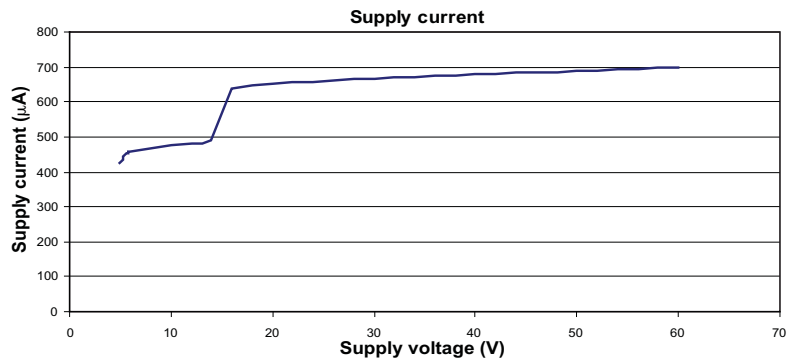
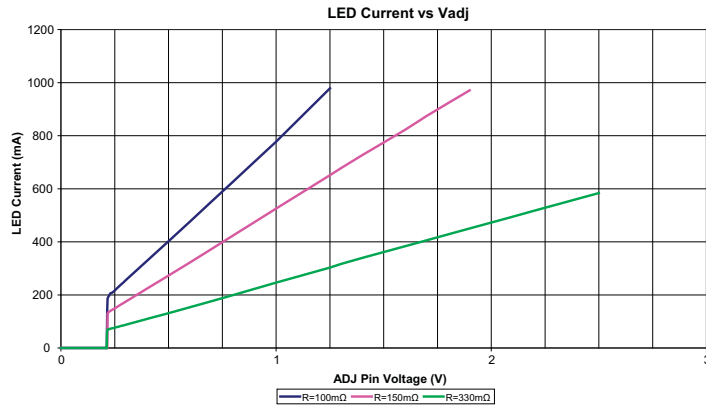


**ZXLD1362 Duty Cycle**  
*L=220µH*

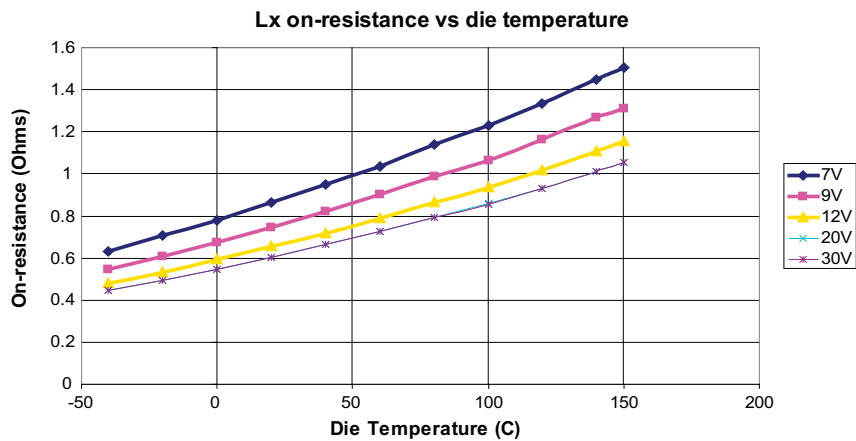
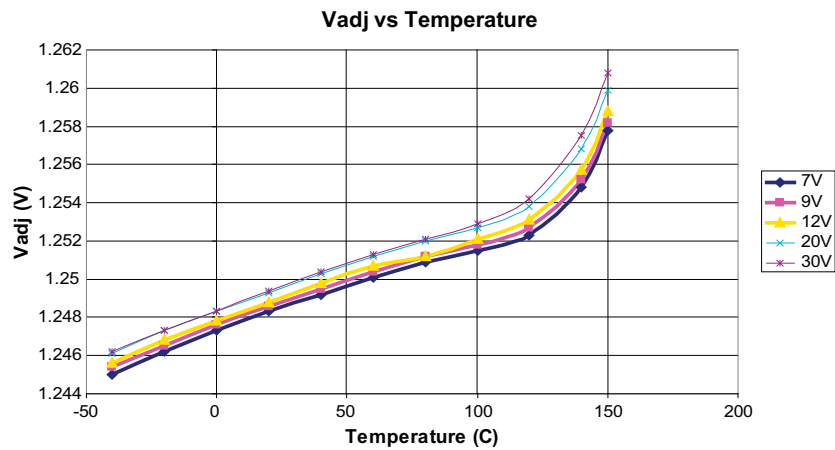
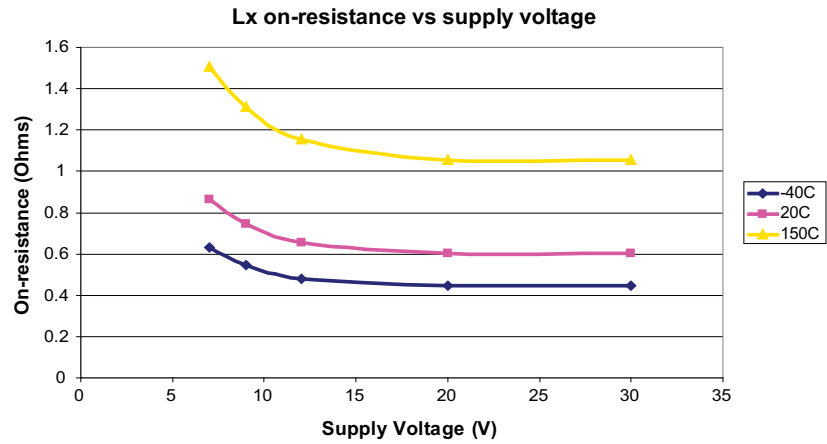




## Typical operating conditions



## Typical operating conditions



## Application notes

### Setting nominal average output current with external resistor $R_S$

The nominal average output current in the LED(s) is determined by the value of the external current sense resistor ( $R_S$ ) connected between  $V_{IN}$  and  $I_{SENSE}$  and is given by:

$$I_{OUTnom} = 0.1/R_S \text{ [for } R_S \geq 0.1\Omega \text{]}$$

The table below gives values of nominal average output current for several preferred values of current setting resistor ( $R_S$ ) in the typical application circuit shown on page 1:

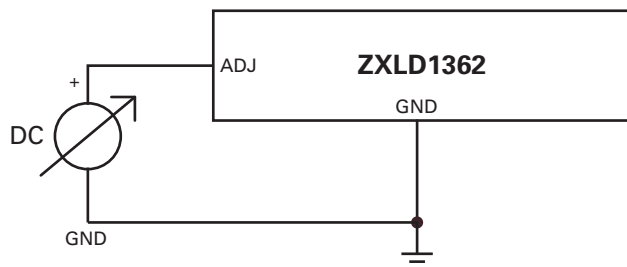
$R_S$ ( $\Omega$ )	Nominal average output current (mA)
0.1	1000
0.13	760
0.15	667

The above values assume that the ADJ pin is floating and at a nominal voltage of  $V_{REF}$  (=1.25V). Note that  $R_S = 0.1\Omega$  is the minimum allowed value of sense resistor under these conditions to maintain switch current below the specified maximum value.

It is possible to use different values of  $R_S$  if the ADJ pin is driven from an external voltage. (See next section).

### Output current adjustment by external DC control voltage

The ADJ pin can be driven by an external dc voltage ( $V_{ADJ}$ ), as shown, to adjust the output current to a value above or below the nominal average value defined by  $R_S$ .



The nominal average output current in this case is given by:

$$I_{OUTdc} = (V_{ADJ} / 1.25) \times 100\text{mV} \times R_S \text{ [for } 0.3 < V_{ADJ} < 2.5\text{V} \text{]}$$

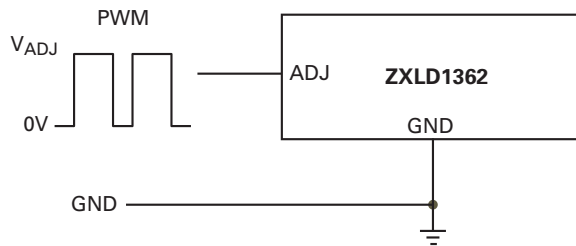
Note that 100% brightness setting corresponds to  $V_{ADJ} = V_{REF}$ . When driving the ADJ pin above 1.25V,  $R_S$  must be increased in proportion to prevent  $I_{OUTdc}$  exceeding 1A maximum.

The input impedance of the ADJ pin is  $50\text{k}\Omega \pm 25\%$  for voltages below  $V_{REF}$  and  $20\text{k}\Omega \pm 25\%$  for voltages above  $V_{REF} + 100\text{mV}$ .

## Output current adjustment by PWM control

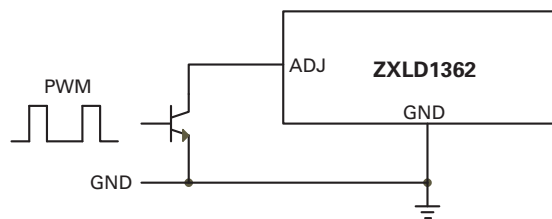
### Directly driving ADJ input

A Pulse Width Modulated (PWM) signal with duty cycle  $D_{PWM}$  can be applied to the ADJ pin, as shown below, to adjust the output current to a value above or below the nominal average value set by resistor  $R_G$ :



### Driving the ADJ input via open collector transistor

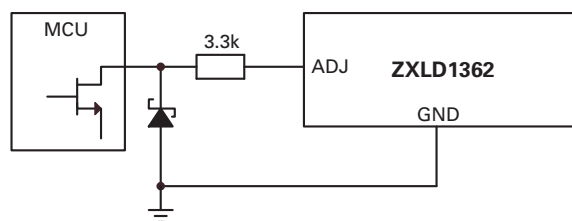
The recommended method of driving the ADJ pin and controlling the amplitude of the PWM waveform is to use a small NPN switching transistor as shown below:



This scheme uses the 50k resistor between the ADJ pin and the internal voltage reference as a pull-up resistor for the external transistor.

### Driving the ADJ input from a microcontroller

Another possibility is to drive the device from the open drain output of a microcontroller. The diagram below shows one method of doing this:



If the NMOS transistor within the microcontroller has high Drain / Source capacitance, this arrangement can inject a negative spike into ADJ input of the 1362 and cause erratic operation but the addition of a Schottky clamp diode (cathode to ADJ) to ground and inclusion of a series resistor (3.3k) will prevent this. See the section on PWM dimming for more details of the various modes of control using high frequency and low frequency PWM signals.

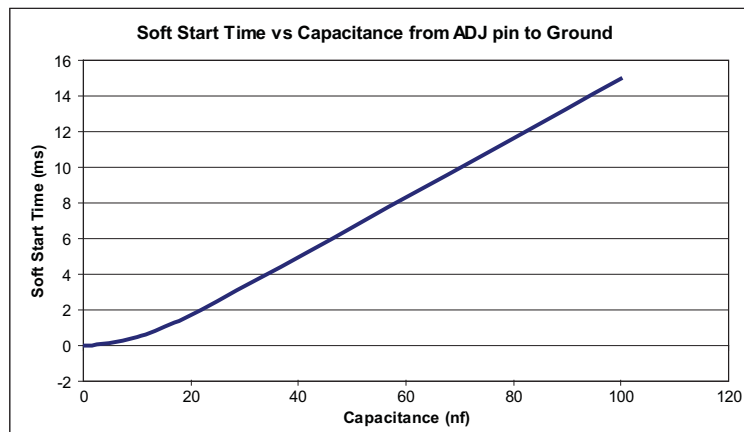
## Shutdown mode

Taking the ADJ pin to a voltage below 0.2V for more than approximately 100µs, will turn off the output and supply current will fall to a low standby level of 60µA nominal.

Note that the ADJ pin is not a logic input. Taking the ADJ pin to a voltage above  $V_{REF}$  will increase output current above the 100% nominal average value. (See graphs for details).

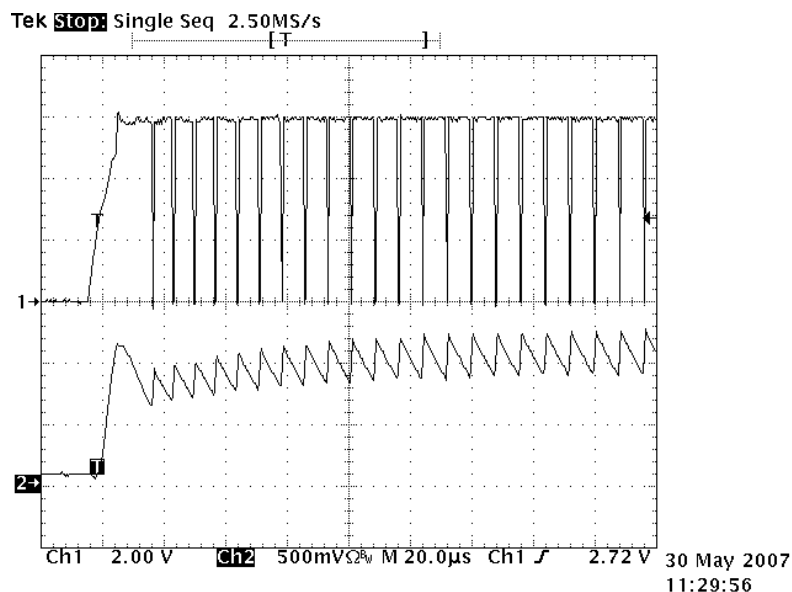
## Soft-start

An external capacitor from the ADJ pin to ground will provide a soft-start delay, by increasing the time taken for the voltage on this pin to rise to the turn-on threshold and by slowing down the rate of rise of the control voltage at the input of the comparator. Adding capacitance increases this delay by approximately 0.2ms/nF. The graph below shows the variation of soft-start time for different values of capacitor.



## Actual operating waveforms [ $V_{IN}=24V$ , $R_S=0.1\Omega$ , $L=68\mu H$ , 22nF on ADJ]

Soft-start operation. Output current (Ch2) and LX voltage (Ch1)



## **V<sub>IN</sub> capacitor selection**

A low ESR capacitor should be used for input decoupling, as the ESR of this capacitor appears in series with the supply source impedance and lowers overall efficiency. This capacitor has to supply the relatively high peak current to the coil and smooth the current ripple on the input supply.

To avoid transients into the IC, the size of the input capacitor will depend on the V<sub>IN</sub> voltage:

$$V_{IN} = 6 \text{ to } 40 \quad C_{IN} = 2.2\mu\text{F}$$

$$V_{IN} = 40 \text{ to } 50 \quad C_{IN} = 4.7\mu\text{F}$$

$$V_{IN} = 50 \text{ to } 60 \quad C_{IN} = 10\mu\text{F}$$

When the input voltage is close to the output voltage the input current increases which puts more demand on the input capacitor. The minimum value of 2.2 $\mu$ F may need to be increased to 4.7 $\mu$ F; higher values will improve performance at lower input voltages, especially when the source impedance is high. The input capacitor should be placed as close as possible to the IC.

For maximum stability over temperature and voltage, capacitors with X7R, X5R, or better dielectric is recommended. Capacitors with Y5V dielectric are not suitable for decoupling in this application and should **NOT** be used.

If higher voltages are used and the C<sub>IN</sub> is 10 $\mu$ F. This can be an electrolytic capacitor provide a suitable 1 $\mu$ F ceramic capacitor is also used and positioned as close the V<sub>IN</sub> of the IC as possible.

A suitable TDK capacitor would be CK657NX7R2AXXM.

The following web sites are useful when finding alternatives:

[www.tdk.com](http://www.tdk.com)

[www.murata.com](http://www.murata.com)

[www.t-yuden.com](http://www.t-yuden.com)

[www.kemet.com](http://www.kemet.com)

[www.avxcorp.com](http://www.avxcorp.com)

## Inductor selection

Recommended inductor values for the ZXLD1362 are in the range 68 $\mu$ H to 220 $\mu$ H.

Higher values of inductance are recommended at higher supply voltages in order to minimize errors due to switching delays, which result in increased ripple and lower efficiency. Higher values of inductance also result in a smaller change in output current over the supply voltage range. (See graphs). The inductor should be mounted as close to the device as possible with low resistance connections to the LX and V<sub>IN</sub> pins.

The chosen coil should have a saturation current higher than the peak output current and a continuous current rating above the required mean output current.

Suitable coils for use with the ZXLD1362 may be selected from the MSS range manufactured by Coilcraft, or the NPIS range manufactured by NIC components.

The inductor value should be chosen to maintain operating duty cycle and switch 'on'/'off' times within the specified limits over the supply voltage and load current range.

The following equations can be used as a guide, with reference to Figure 1 - Operating waveforms.

## LX Switch 'On' time

$$T_{ON} = \frac{L\Delta I}{V_{IN} - V_{LED} - I_{avg}(R_S + rL + R_{LX})}$$

Note:  $T_{ONmin} > 240ns$

## LX Switch 'Off' time

$$T_{OFF} = \frac{L\Delta I}{V_{LED} + V_D + I_{avg}(R_S + rL)}$$

Note:  $T_{OFFmin} > 200ns$

### Where:

L is the coil inductance (H)

rL is the coil resistance ( $\Omega$ )

$R_S$  is the current sense resistance

$I_{avg}$  is the required LED current (A)

$\Delta I$  is the coil peak-peak ripple current (A) {Internally set to  $0.3 \times I_{avg}$ }

$V_{IN}$  is the supply voltage (V)

$V_{LED}$  is the total LED forward voltage (V)

$R_{LX}$  is the switch resistance ( $\Omega$ ) {=0.5 $\Omega$  nominal}

$V_D$  is the diode forward voltage at the required load current (V)

### Example:

For  $V_{IN} = 24V$ ,  $L = 68\mu H$ ,  $rL = 0.034\Omega$ ,  $R_S = 0.1\Omega$ ,  $R_{LX} = 0.5\Omega$ ,  $V_{LED} = 3.6V \times 3$ ,  $I_{avg} = 1A$  and  $V_D = 0.49V$

$$T_{ON} = (68e-6 \times 0.3) / (24 - 10.8 - 0.904) = 1.66\mu s$$

$$T_{OFF} = (68e-6 \times 0.3) / (10.8 + 0.49 + 0.404) = 1.75\mu s$$

This gives an operating frequency of 294 kHz and a duty cycle of 0.49.

These and other equations are available as a spreadsheet calculator from the Zetex website at [www.zetex.com/zxld1362](http://www.zetex.com/zxld1362)

Note that, in practice, the duty cycle and operating frequency will deviate from the calculated values due to dynamic switching delays, switch rise/fall times and losses in the external components.

Optimum performance will be achieved by setting the duty cycle close to 0.5 at the nominal supply voltage. This helps to equalize the undershoot and overshoot and improves temperature stability of the output current.



## Diode selection

For maximum efficiency and performance, the rectifier (D1) should be a fast low capacitance Schottky diode with low reverse leakage at the maximum operating voltage and temperature.

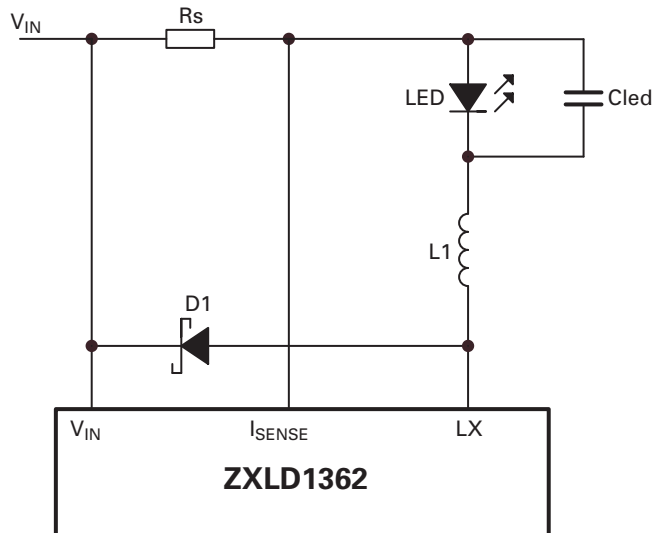
They also provide better efficiency than silicon diodes, due to a combination of lower forward voltage and reduced recovery time.

It is important to select parts with a peak current rating above the peak coil current and a continuous current rating higher than the maximum output load current. It is very important to consider the reverse leakage of the diode when operating above 85°C. Excess leakage will increase the power dissipation in the device and if close to the load may create a thermal runaway condition.

The higher forward voltage and overshoot due to reverse recovery time in silicon diodes will increase the peak voltage on the LX output. If a silicon diode is used, care should be taken to ensure that the total voltage appearing on the LX pin including supply ripple, does not exceed the specified maximum value.

## Reducing output ripple

Peak to peak ripple current in the LED(s) can be reduced, if required, by shunting a capacitor  $C_{led}$  across the LED(s) as shown below:



A value of  $1\mu F$  will reduce the supply ripple current by a factor three (approx.). Proportionally lower ripple can be achieved with higher capacitor values. Note that the capacitor will not affect operating frequency or efficiency, but it will increase start-up delay, by reducing the rate of rise of LED voltage.

By adding this capacitor the current waveform through the LED(s) changes from a triangular ramp to a more sinusoidal version without altering the mean current value .

## Operation at low supply voltage

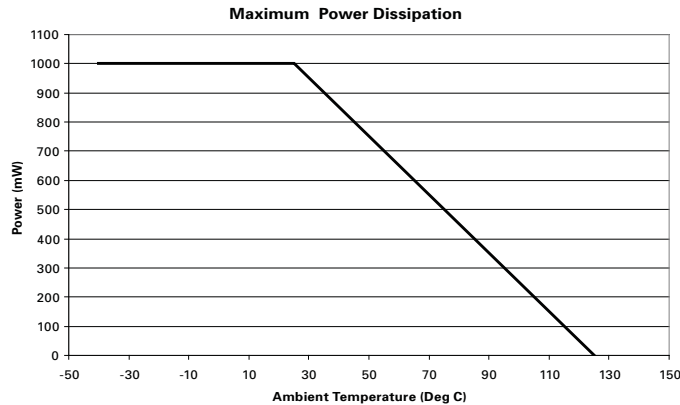
Below the under-voltage lockout threshold ( $V_{SD}$ ) the drive to the output transistor is turned off to prevent device operation with excessive on-resistance of the output transistor. The output transistor is not full enhanced until the supply voltage exceeds approximately 17V. At supply voltages between  $V_{SD}$  and 17V care must be taken to avoid excessive power dissipation due to the on-resistance.

If the supply voltage is always less than 30V continuous (or less than 40V for less than 0.5s) an alternative device is available, the ZXLD1360.

Note that when driving loads of two or more LEDs, the forward drop will normally be sufficient to prevent the device from switching below approximately 6V. This will minimize the risk of damage to the device.

## Thermal considerations

When operating the device at high ambient temperatures, or when driving maximum load current, care must be taken to avoid exceeding the package power dissipation limits. The graph below gives details for power derating. This assumes the device to be mounted on a  $25\text{mm}^2$  PCB with 1oz copper standing in still air.



Note that the device power dissipation will most often be a maximum at minimum supply voltage. It will also increase if the efficiency of the circuit is low. This may result from the use of unsuitable coils, or excessive parasitic output capacitance on the switch output.

### Thermal compensation of output current

High luminance LEDs often need to be supplied with a temperature compensated current in order to maintain stable and reliable operation at all drive levels. The LEDs are usually mounted remotely from the device so, for this reason, the temperature coefficients of the internal circuits for the ZXLD1362 have been optimized to minimize the change in output current when no compensation is employed. If output current compensation is required, it is possible to use an external temperature sensing network - normally using Negative Temperature Coefficient (NTC) thermistors and/or diodes, mounted very close to the LED(s). The output of the sensing network can be used to drive the ADJ pin in order to reduce output current with increasing temperature.

## Layout considerations

### LX pin

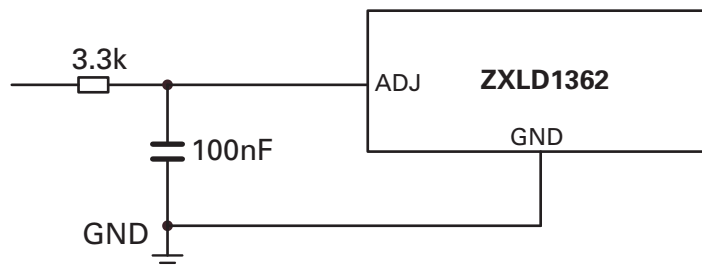
The LX pin of the device is a fast switching node, so PCB tracks should be kept as short as possible. To minimize ground 'bounce', the ground pin of the device should be soldered directly to the ground plane.

### Coil and decoupling capacitors and current sense resistor

It is particularly important to mount the coil and the input decoupling capacitor as close to the device pins as possible to minimize parasitic resistance and inductance, which will degrade efficiency. It is also important to minimize any track resistance in series with current sense resistor  $R_S$ . Its best to connect  $V_{IN}$  directly to one end of  $R_S$  and  $I_{sense}$  directly to the opposite end of  $R_S$  with no other currents flowing in these tracks. It is important that the cathode current of the Schottky diode does not flow in a track between  $R_S$  and  $V_{IN}$  as this may give an apparent higher measure of current than is actual because of track resistance.

### ADJ pin

The ADJ pin is a high impedance input for voltages up to 1.35V so, when left floating, PCB tracks to this pin should be as short as possible to reduce noise pickup. A 100nF capacitor from the ADJ pin to ground will reduce frequency modulation of the output under these conditions. An additional series 3.3k $\Omega$  resistor can also be used when driving the ADJ pin from an external circuit (see below). This resistor will provide filtering for low frequency noise and provide protection against high voltage transients.



### High voltage tracks

Avoid running any high voltage tracks close to the ADJ pin, to reduce the risk of leakage currents due to board contamination. The ADJ pin is soft-clamped for voltages above 1.35V to desensitize it to leakage that might raise the ADJ pin voltage and cause excessive output current. However, a ground ring placed around the ADJ pin is recommended to minimize changes in output current under these conditions.

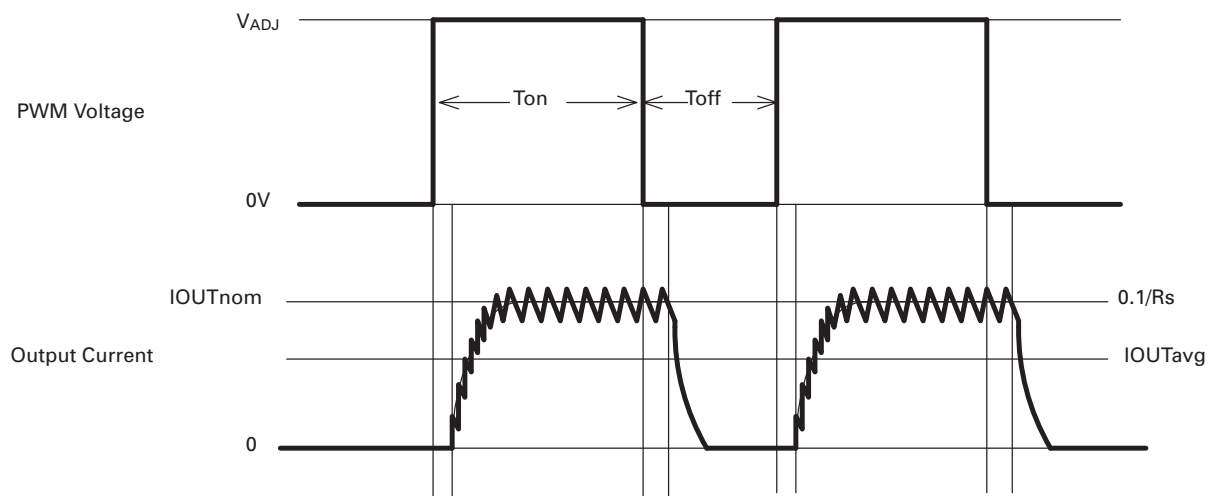
### Evaluation PCB

ZXLD1362 evaluation boards are available on request. These boards contain LEDs to allow quick testing of the 1362 device. Additional terminals allow for interfacing to customers own LED products.

## Dimming output current using PWM

### Low frequency PWM mode

When the ADJ pin is driven with a low frequency PWM signal (eg 100Hz), with a high level voltage  $V_{ADJ}$  and a low level of zero, the output of the internal low pass filter will swing between 0V and  $V_{ADJ}$ , causing the input to the shutdown circuit to fall below its turn-off threshold (200mV nom) when the ADJ pin is low. This will cause the output current to be switched on and off at the PWM frequency, resulting in an average output current  $I_{OUTavg}$  proportional to the PWM duty cycle. (See Figure 2 - Low frequency PWM operating waveforms).



**Figure 2 Low frequency PWM operating waveforms**

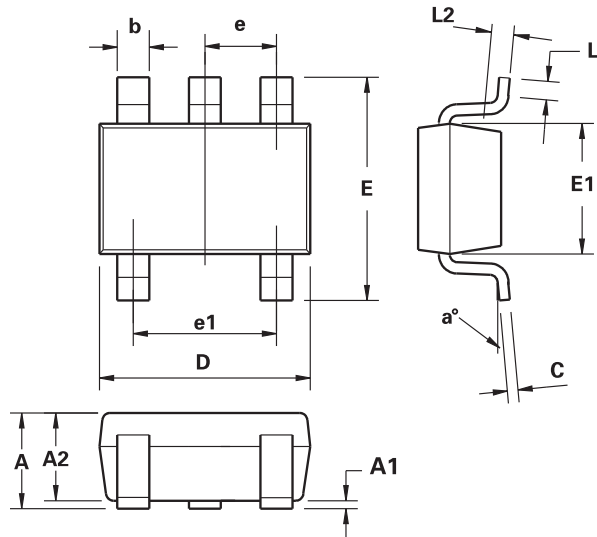
The average value of output current in this mode is given by:

$$I_{OUTavg} = 0.1 D_{PWM} / R_S \text{ [for } D_{PWM} > 0.001 \text{]}$$

This mode is preferable if optimum LED 'whiteness' is required. It will also provide the widest possible dimming range (approx. 1000:1) and higher efficiency at the expense of greater output ripple.

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## Package outline - TSOT23-5



DIM	Millimeters		Inches	
	Min.	Max.	Min.	Max.
A	-	1.00	-	0.0393
A1	0.01	0.10	0.0003	0.0039
A2	0.84	0.90	0.0330	0.0354
b	0.30	0.45	0.0118	0.0177
c	0.12	0.20	0.0047	0.0078
D	2.90 BSC		0.114 BSC	
E	2.80 BSC		0.110 BSC	
E1	1.60 BSC		0.062 BSC	
e	0.95 BSC		0.0374 BSC	
e1	1.90 BSC		0.0748 BSC	
L	0.30	0.50	0.0118	0.0196
L2	0.25 BSC		0.010 BSC	
a°	4°	12°	4°	12°

**Note:** Controlling dimensions are in millimeters. Approximate dimensions are provided in inches

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"Not recommended for new designs"	Device is still in production to support existing designs and production
"Obsolete"	Production has been discontinued

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### Zetex sales offices

Europe	Americas	Asia Pacific	Corporate Headquarters
Zetex GmbH Kustermann-park Balanstraße 59 D-81541 München Germany Telephone: (49) 89 45 49 49 0 Fax: (49) 89 45 49 49 49 europe.sales@zetex.com	Zetex Inc 700 Veterans Memorial Highway Hauppauge, NY 11788 USA Telephone: (1) 631 360 2222 Fax: (1) 631 360 8222 usa.sales@zetex.com	Zetex (Asia Ltd) 3701-04 Metroplaza Tower 1 Hing Fong Road, Kwai Fong Hong Kong Telephone: (852) 26100 611 Fax: (852) 24250 494 asia.sales@zetex.com	Zetex Semiconductors plc Zetex Technology Park, Chadderton Oldham, OL9 9LL United Kingdom Telephone: (44) 161 622 4444 Fax: (44) 161 622 4446 hq@zetex.com

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