



SBOS019A - JANUARY 1992 - SEPTEMBER 2003

# **FET-Input, Low Distortion OPERATIONAL AMPLIFIER**

# **FEATURES**

● LOW DISTORTION: 0.0003% at 1kHz

● LOW NOISE: 10nV/√Hz ● HIGH SLEW RATE: 25V/μs

WIDE GAIN-BANDWIDTH: 20MHz

• UNITY-GAIN STABLE

• WIDE SUPPLY RANGE:  $V_s = \pm 4.5$  to  $\pm 24V$ 

DRIVES 600Ω LOAD

DUAL VERSION AVAILABLE (OPA2604)

# DESCRIPTION

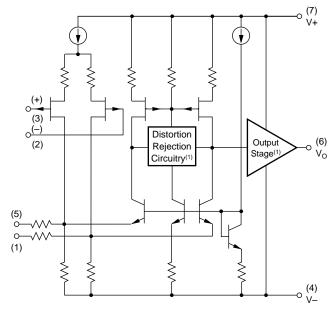
The OPA604 is a FET-input operational amplifier designed for enhanced AC performance. Very low distortion, low noise and wide bandwidth provide superior performance in high quality audio and other applications requiring excellent dynamic performance.

New circuit techniques and special laser trimming of dynamic circuit performance yield very low harmonic distortion. The result is an op amp with exceptional sound quality. The lownoise FET input of the OPA604 provides wide dynamic range, even with high source impedance. Offset voltage is laser-trimmed to minimize the need for interstage coupling

The OPA604 is available in 8-pin plastic mini-DIP and SO-8 surface-mount packages, specified for the -25°C to +85°C temperature range.

## APPLICATIONS

- PROFESSIONAL AUDIO EQUIPMENT
- **PCM DAC I/V CONVERTERS**
- SPECTRAL ANALYSIS EQUIPMENT
- ACTIVE FILTERS
- TRANSDUCER AMPLIFIERS
- **DATA ACQUISITION**



NOTE: (1) Patents Granted: #5053718, 5019789



Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

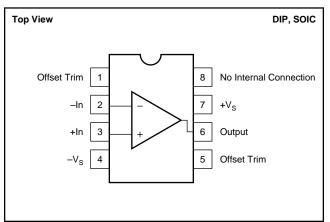
All trademarks are the property of their respective owners.



## **ABSOLUTE MAXIMUM RATINGS**

Power Supply Voltage	±25V
Input Voltage	(V–)–1V to (V+)+1V
Output Short Circuit to Ground	
Operating Temperature	–40°C to +100°C
Storage Temperature	40°C to +125°C
Junction Temperature	+150°C
Lead Temperature (soldering, 10s) AP	+300°C
Lead Temperature (soldering, 3s) AU	+260°C

#### **PIN CONFIGURATION**





Any integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet published specifications.

### PACKAGE/ORDERING INFORMATION

For the most current package and ordering information, see to the Package Option Addendum at the end of this data sheet.



# **ELECTRICAL CHARACTERISTICS**

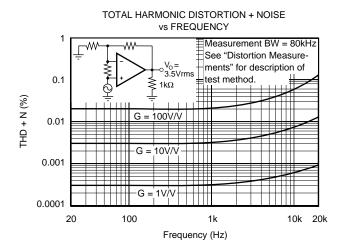
 $T_A$  = +25°C,  $V_S$  = ±15V, unless otherwise noted.

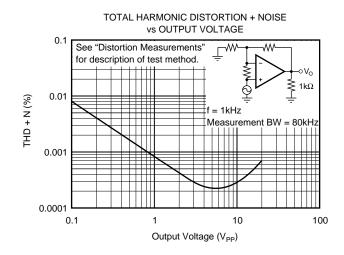
		OPA604AP, AU			
PARAMETER	CONDITION	MIN	TYP	MAX	UNITS
OFFSET VOLTAGE Input Offset Voltage Average Drift Power Supply Rejection	V <sub>S</sub> = ±5 to ±24V	80	±1 ±8 100	±5	mV μV/°C dB
INPUT BIAS CURRENT <sup>(1)</sup> Input Bias Current Input Offset Current	$V_{CM} = 0V$ $V_{CM} = 0V$		50 ±3		pA pA
NOISE Input Voltage Noise Noise Density: f = 10Hz f = 100Hz f = 1kHz f = 10kHz Voltage Noise, BW = 20Hz to 20kHz Input Bias Current Noise Current Noise Density, f = 0.1Hz to 20kHz			25 15 11 10 1.5		nV/√Hz nV/√Hz nV/√Hz nV/√Hz μV <sub>PP</sub> fA/√Hz
INPUT VOLTAGE RANGE Common-Mode Input Range Common-Mode Rejection	V <sub>CM</sub> = ±12V	±12 80	±13 100		V dB
INPUT IMPEDANCE Differential Common-Mode			10 <sup>12</sup>    8 10 <sup>12</sup>    10		Ω    pF Ω    pF
OPEN-LOOP GAIN Open-Loop Voltage Gain	$V_O = \pm 10V, R_L = 1k\Omega$	80	100		dB
FREQUENCY RESPONSE Gain-Bandwidth Product Slew Rate Settling Time: 0.01% 0.1% Total Harmonic Distortion + Noise (THD+N)	$G = 100$ $20V_{PP}, R_{L} = 1k\Omega$ $G = -1, 10V \text{ Step}$ $G = 1, f = 1kHz$	15	20 25 1.5 1 0.0003		MHz V/μs μs μs %
OUTPUT Voltage Output Current Output Short Circuit Current Output Resistance, Open-Loop	$V_O = 3.5 V \text{rms}, R_L = 1 \text{k}\Omega$ $R_L = 600\Omega$ $V_O = \pm 12 V$	±11	±12 ±35 ±40 25		V mA mA Ω
POWER SUPPLY Specified Operating Voltage Operating Voltage Range Current		±4.5	±15 ±5.3	±24 ±7	V V mA
<b>TEMPERATURE RANGE</b> Specification Storage Thermal Resistance <sup>(2)</sup> , $\theta_{\rm JA}$		-25 -40	90	+85 +125	%C % %C

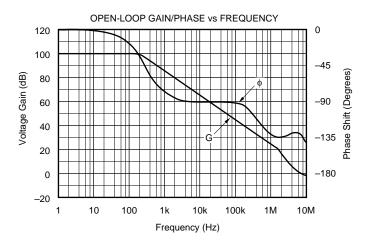
NOTES: (1) Typical performance, measured fully warmed-up. (2) Soldered to circuit board—see text.

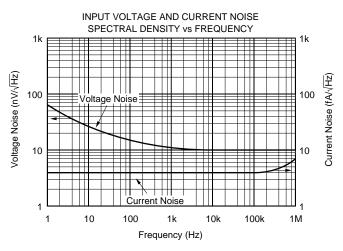
# TYPICAL CHARACTERISTICS

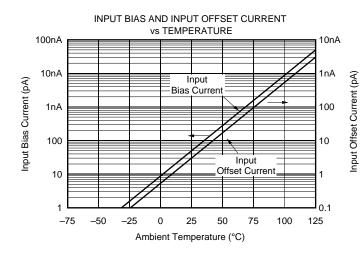
 $T_A = +25$ °C,  $V_S = \pm 15$ V, unless otherwise noted.

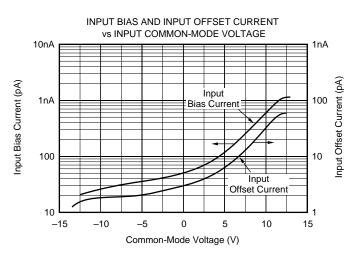






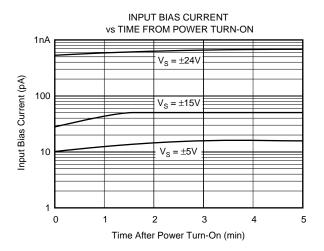


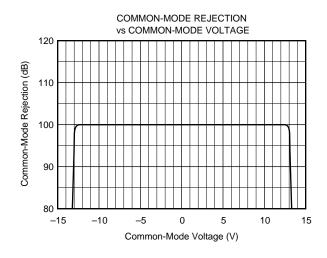


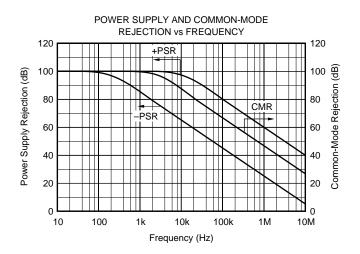


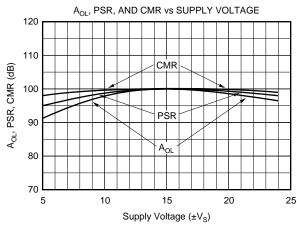
# TYPICAL CHARACTERISTICS (Cont.)

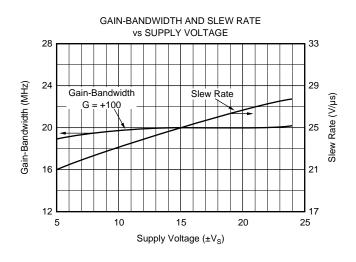
 $T_A = +25$ °C,  $V_S = \pm 15$ V, unless otherwise noted.

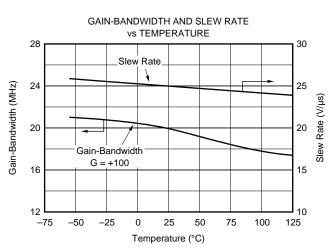






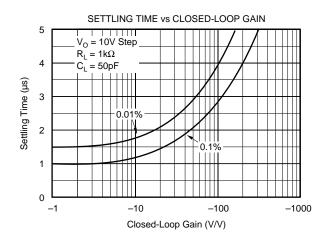


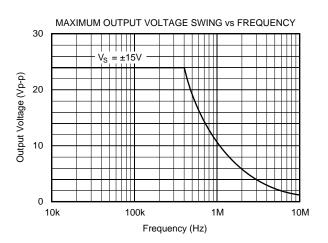


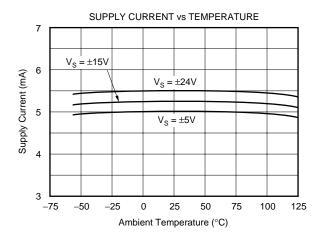


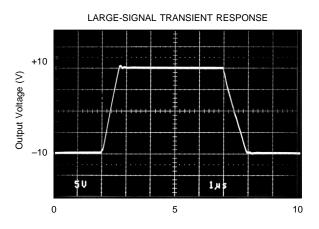
# **TYPICAL CHARACTERISTICS (Cont.)**

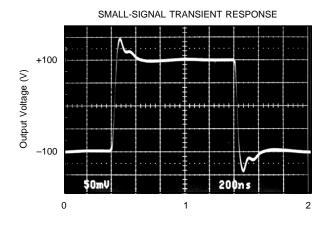
 $T_A = +25$ °C,  $V_S = \pm 15$ V, unless otherwise noted.

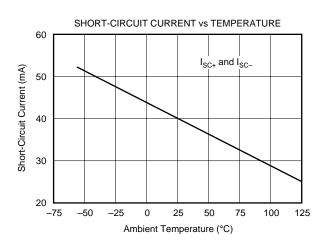








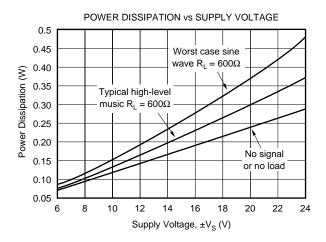


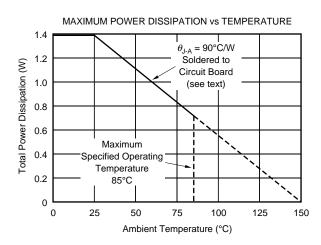




# TYPICAL CHARACTERISTICS (Cont.)

 $T_A = +25$ °C,  $V_S = \pm 15$ V, unless otherwise noted.





# **APPLICATIONS INFORMATION**

## **OFFSET VOLTAGE ADJUSTMENT**

The OPA604 offset voltage is laser-trimmed and will require no further trim for most applications. As with most amplifiers, externally trimming the remaining offset can change drift performance by about  $0.3\mu V/^{\circ}C$  for each  $100\mu V$  of adjusted offset. The OPA604 can replace many other amplifiers by leaving the external null circuit unconnected.

The OPA604 is unity-gain stable, making it easy to use in a wide range of circuitry. Applications with noisy or high impedance power supply lines may require decoupling capacitors close to the device pins. In most cases, a  $1\mu F$  tantalum capacitor at each power supply pin is adequate.

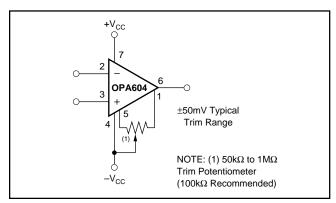


FIGURE 1. Offset Voltage Trim.

### **DISTORTION MEASUREMENTS**

The distortion produced by the OPA604 is below the measurement limit of virtually all commercially available equipment. A special test circuit, however, can be used to extend the measurement capabilities.

Op amp distortion can be considered an internal error source which can be referred to the input. Figure 2 shows a circuit which causes the op amp distortion to be 101 times greater than normally produced by the op amp. The addition of  $R_3$  to the otherwise standard noninverting amplifier configuration alters the feedback factor or noise gain of the circuit. The closed-loop gain is unchanged, but the feedback available for error correction is reduced by a factor of 101. This extends the measurement limit, including the effects of the signal-source purity, by a factor of 101. Note that the input signal and load applied to the op amp are the same as with conventional feedback without  $R_3$ .

Validity of this technique can be verified by duplicating measurements at high gain and/or high frequency where the distortion is within the measurement capability of the test equipment. Measurements for this data sheet were made with the Audio Precision System One, which greatly simplifies such repetitive measurements. The measurement technique can, however, be performed with manual distortion measurement instruments.

#### **CAPACITIVE LOADS**

The dynamic characteristics of the OPA604 have been optimized for commonly encountered gains, loads and operating conditions. The combination of low closed-loop gain and capacitive load will decrease the phase margin and may lead to gain peaking or oscillations. Load capacitance reacts with the op amp's open-loop output resistance to form an additional pole in the feedback loop. Figure 3 shows various circuits which preserve phase margin with capacitive load. For details of analysis techniques and applications circuits, refer to application bulletin AB-028 (SBOA015) located at www.ti.com.



For the unity-gain buffer, Figure 3a, stability is preserved by adding a phase-lead network,  $R_{\rm C}$  and  $C_{\rm C}$ . Voltage drop across  $R_{\rm C}$  will reduce output voltage swing with heavy loads. An alternate circuit, Figure 3b, does not limit the output with low load impedance. It provides a small amount of positive feedback to reduce the net feedback factor. Input impedance of this circuit falls at high frequency as op amp gain rolloff reduces the bootstrap action on the compensation network.

Figures 3c and 3d show compensation techniques for noninverting amplifiers. Like the follower circuits, the circuit in Figure 3d eliminates voltage drop due to load current, but at the penalty of somewhat reduced input impedance at high frequency.

Figures 3e and 3f show input lead compensation networks for inverting and difference amplifier configurations.

#### **NOISE PERFORMANCE**

Op amp noise is described by two parameters—noise voltage and noise current. The voltage noise determines the noise performance with low source impedance. Low noise bipolar-input op amps such as the OPA27 and OPA37 provide very low voltage noise. But if source impedance is greater than a few thousand ohms, the current noise of

bipolar-input op amps react with the source impedance and will dominate. At a few thousand ohms source impedance and above, the OPA604 will generally provide lower noise.

#### POWER DISSIPATION

The OPA604 is capable of driving a  $600\Omega$  load with power-supply voltages up to  $\pm 24$ V. Internal power dissipation is increased when operating at high power supply voltage. The typical characteristic curve, Power Dissipation vs Power Supply Voltage, shows quiescent dissipation (no signal or no load) as well as dissipation with a worst case continuous sine wave. Continuous high-level music signals typically produce dissipation significantly less than worst-case sine waves.

Copper leadframe construction used in the OPA604 improves heat dissipation compared to conventional plastic packages. To achieve best heat dissipation, solder the device directly to the circuit board and use wide circuit board traces.

#### **OUTPUT CURRENT LIMIT**

Output current is limited by internal circuitry to approximately ±40mA at 25°C. The limit current decreases with increasing temperature as shown in the typical curves.

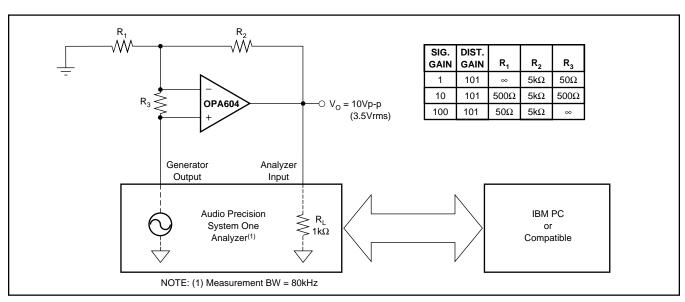


FIGURE 2. Distortion Test Circuit.

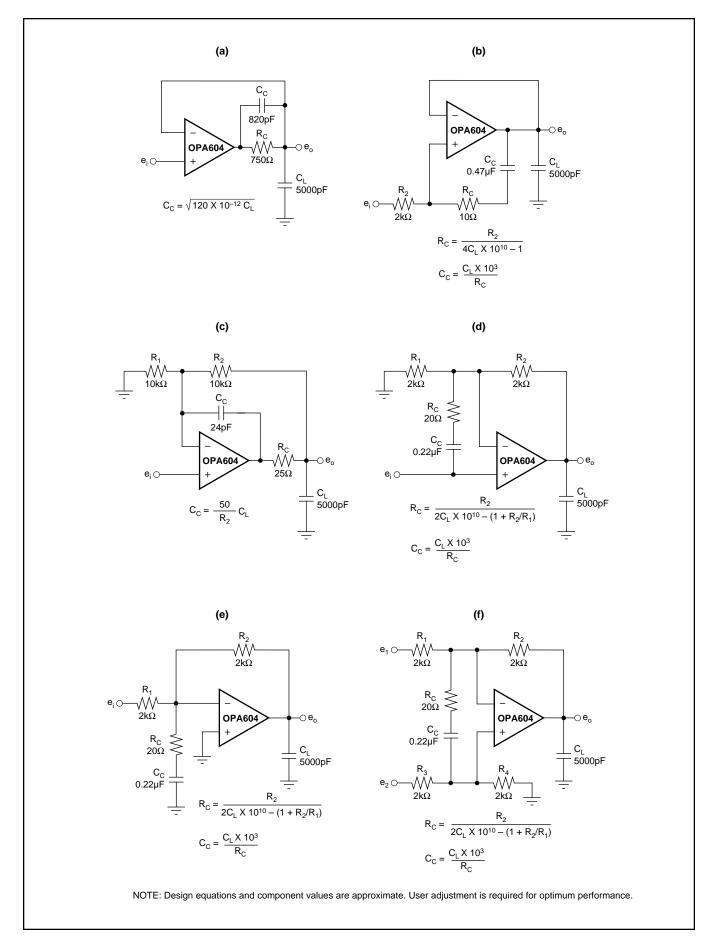


FIGURE 3. Driving Large Capacitive Loads.

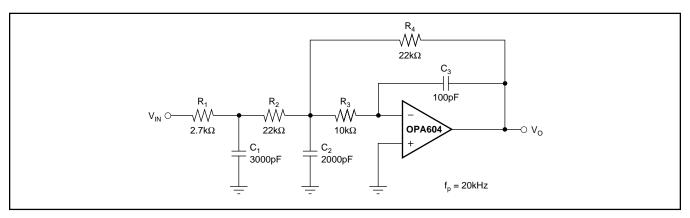


FIGURE 4. Three-Pole Low-Pass Filter.

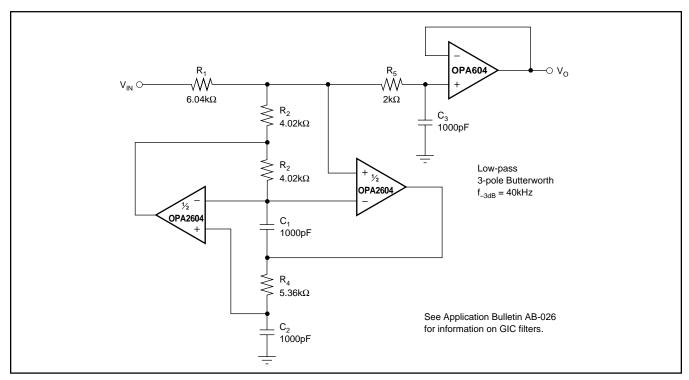


FIGURE 5. Three-Pole Generalized Immittance Converter (GIC) Low-Pass Filter.

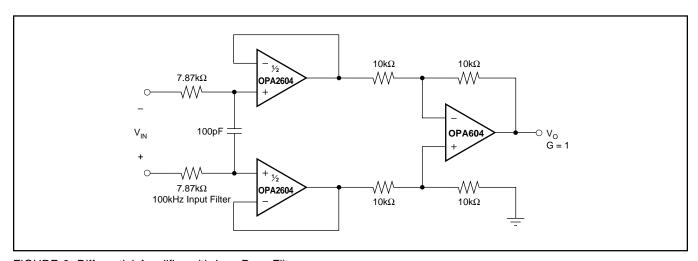
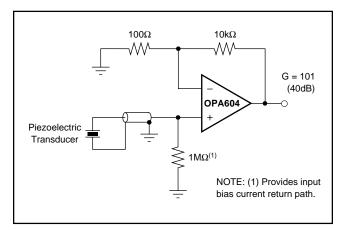


FIGURE 6. Differential Amplifier with Low-Pass Filter.





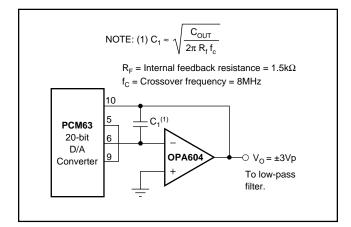


FIGURE 7. High Impedance Amplifier.

FIGURE 8. Digital Audio DAC I-V Amplifier.

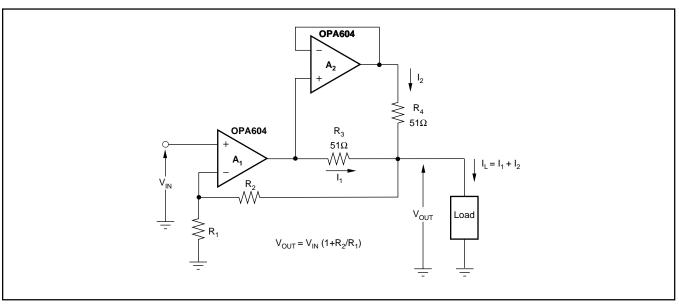


FIGURE 9. Using Two OPA604 Op Amps to Double the Output Current to a Load.

# **SOUND QUALITY**

The following discussion is provided, recognizing that not all measured performance behavior explains or correlates with listening tests by audio experts. The design of the OPA604 included consideration of both objective performance measurements, as well as an awareness of widely held theory on the success and failure of previous op amp designs.

#### **SOUND QUALITY**

The sound quality of an op amp is often the crucial selection criteria—even when a data sheet claims exceptional distortion performance. By its nature, sound quality is subjective. Furthermore, results of listening tests can vary depending on application and circuit configuration. Even experienced listeners in controlled tests often reach different conclusions.

Many audio experts believe that the sound quality of a high performance FET op amp is superior to that of bipolar op amps. A possible reason for this is that bipolar designs generate greater odd-order harmonics than FETs. To the human ear, odd-order harmonics have long been identified as sounding more unpleasant than even-order harmonics. FETs, like vacuum tubes, have a square-law I-V transfer function which is more linear than the exponential transfer function of a bipolar transistor. As a direct result of this square-law characteristic, FETs produce predominantly even-order harmonics. Figure 10 shows the transfer function of a bipolar transistor and FET. Fourier transformation of both transfer functions reveals the lower odd-order harmonics of the FET amplifier stage.

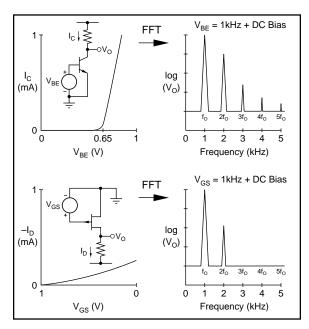
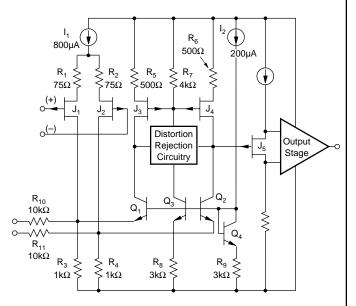


FIGURE 10. I-V and Spectral Response of NPN and JFET.



#### THE OPA604 DESIGN

The OPA604 uses FETs throughout the signal path, including the input stage, input-stage load, and the important phase-splitting section of the output stage. Bipolar transistors are used where their attributes, such as current capability are important, and where their transfer characteristics have minimal impact.

The topology consists of a single folded-cascode gain stage followed by a unity-gain output stage. Differential input transistors  $J_1$  and  $J_2$  are special large-geometry, P-channel JFETs. Input stage current is a relatively high  $800\mu A$ , providing high transconductance and reducing voltage noise. Laser trimming of stage currents and careful attention to symmetry yields a nearly symmetrical slew rate of  $\pm 25 V/\mu s$ .

The JFET input stage holds input bias current to approximately 50pA or roughly 3000 times lower than common bipolar-input audio op amps. This dramatically reduces noise with high-impedance circuitry.

The drains of  $J_1$  and  $J_2$  are cascoded by  $Q_1$  and  $Q_2$ , driving the input stage loads, FETs  $J_3$  and  $J_4$ . Distortion reduction circuitry (patented) linearizes the open-loop response and increases voltage gain. The 20MHz bandwidth of the OPA604 further reduces distortion through the user-connected feedback loop.

The output stage consists of a JFET phase-splitter loaded into high speed all-NPN output drivers. Output transistors are biased by a special circuit to prevent cutoff, even with full output swing into  $600\Omega$  loads.







ww.ti.com 3-Oct-2003

## **PACKAGING INFORMATION**

ORDERABLE DEVICE	STATUS(1)	PACKAGE TYPE	PACKAGE DRAWING	PINS	PACKAGE QTY
OPA604AP	ACTIVE	PDIP	Р	8	50
OPA604AU	ACTIVE	SOIC	D	8	100
OPA604AU/2K5	ACTIVE	SOIC	D	8	2500

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in

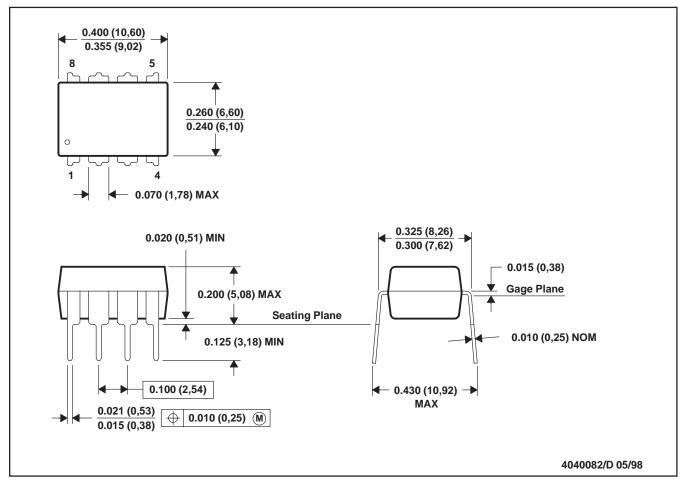
a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

## P (R-PDIP-T8)

## PLASTIC DUAL-IN-LINE



NOTES: A. All linear dimensions are in inches (millimeters).

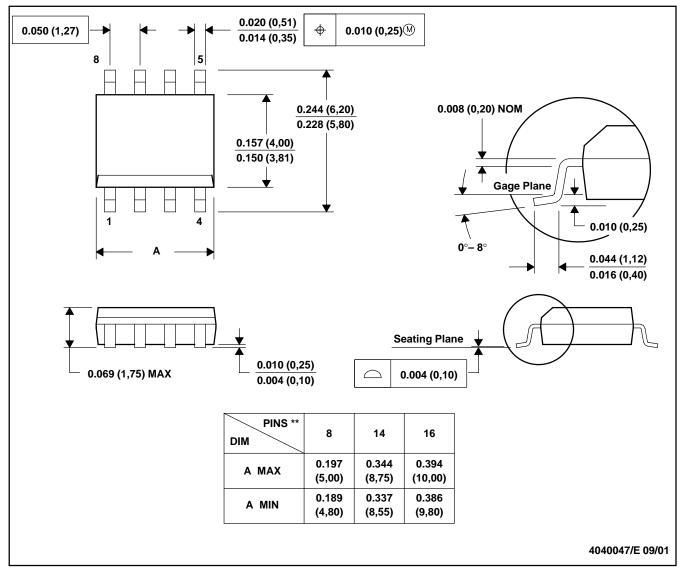
- B. This drawing is subject to change without notice.
- C. Falls within JEDEC MS-001

For the latest package information, go to http://www.ti.com/sc/docs/package/pkg\_info.htm

## D (R-PDSO-G\*\*)

## PLASTIC SMALL-OUTLINE PACKAGE

## **8 PINS SHOWN**



NOTES: A. All linear dimensions are in inches (millimeters).

B. This drawing is subject to change without notice.

C. Body dimensions do not include mold flash or protrusion, not to exceed 0.006 (0,15).

D. Falls within JEDEC MS-012

#### **IMPORTANT NOTICE**

Texas Instruments Incorporated and its subsidiaries (TI) reserve the right to make corrections, modifications, enhancements, improvements, and other changes to its products and services at any time and to discontinue any product or service without notice. Customers should obtain the latest relevant information before placing orders and should verify that such information is current and complete. All products are sold subject to TI's terms and conditions of sale supplied at the time of order acknowledgment.

TI warrants performance of its hardware products to the specifications applicable at the time of sale in accordance with TI's standard warranty. Testing and other quality control techniques are used to the extent TI deems necessary to support this warranty. Except where mandated by government requirements, testing of all parameters of each product is not necessarily performed.

TI assumes no liability for applications assistance or customer product design. Customers are responsible for their products and applications using TI components. To minimize the risks associated with customer products and applications, customers should provide adequate design and operating safeguards.

TI does not warrant or represent that any license, either express or implied, is granted under any TI patent right, copyright, mask work right, or other TI intellectual property right relating to any combination, machine, or process in which TI products or services are used. Information published by TI regarding third-party products or services does not constitute a license from TI to use such products or services or a warranty or endorsement thereof. Use of such information may require a license from a third party under the patents or other intellectual property of the third party, or a license from TI under the patents or other intellectual property of TI.

Reproduction of information in TI data books or data sheets is permissible only if reproduction is without alteration and is accompanied by all associated warranties, conditions, limitations, and notices. Reproduction of this information with alteration is an unfair and deceptive business practice. TI is not responsible or liable for such altered documentation.

Resale of TI products or services with statements different from or beyond the parameters stated by TI for that product or service voids all express and any implied warranties for the associated TI product or service and is an unfair and deceptive business practice. TI is not responsible or liable for any such statements.

Following are URLs where you can obtain information on other Texas Instruments products and application solutions:

Products		Applications	
Amplifiers	amplifier.ti.com	Audio	www.ti.com/audio
Data Converters	dataconverter.ti.com	Automotive	www.ti.com/automotive
DSP	dsp.ti.com	Broadband	www.ti.com/broadband
Interface	interface.ti.com	Digital Control	www.ti.com/digitalcontrol
Logic	logic.ti.com	Military	www.ti.com/military
Power Mgmt	power.ti.com	Optical Networking	www.ti.com/opticalnetwork
Microcontrollers	microcontroller.ti.com	Security	www.ti.com/security
		Telephony	www.ti.com/telephony
		Video & Imaging	www.ti.com/video
		Wireless	www.ti.com/wireless

Mailing Address: Texas Instruments

Post Office Box 655303 Dallas, Texas 75265

Copyright © 2003, Texas Instruments Incorporated